NASA Contractor Report 3316



Modular Antenna Design Study

John W. Ribble

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NASA Contractor Report 3316

Modular Antenna Design Study

John W. Ribble Lockheed Missiles and Space Company, Inc. Sunnyvale, California

Prepared for Langley Research Center under Contract NAS1-14887



Scientific and Technical Information Branch

D.

PREFACE

This report documents the findings of a study funded as Subtask 14 of Contract NAS1-14887. The study researched the mechanical design of a modular antenna concept using a particular deployable module concept. The design was developed sufficiently to allow manufacture of a working demonstration model of a module, and to predict mass properties and to make performance estimates for antenna reflectors composed of these modules.

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1.0 INTRODUCTION

Within the aerospace community, many ways are currently being investigated to assemble, erect, or deploy large reflector surfaces in space. One concept, potentially applicable to the construction of reflectors up to several hundred meters in diameter and embodying several desirable features, consists of individual deployable modules which are assembled in orbit into the final structural configuration. The primary features of this concept are: 1) each module is an autonomous structural element which can be attached to adjacent modules through a three point connection; 2) the upper surface is a folding hexagonal truss plate mechanism which serves as the supporting substructure for a reflective surface; and 3) the entire truss and surface can be folded into a cylindrical envelope in which all truss elements are essentially parallel. The folded module is only 25 cm in diameter and when a full bay length of 17 m is used the deployed module is 24 m across flats. The modules are transported in the folded position, individually deployed on-orbit, and assembled into the required structure.

The initial effort described in this study has accomplished demonstration of concept feasibility through development of a subscale engineering model. This model possesses all mechanical working features such as folding joints, module attachment points, deployment mechanisms, and surface attachment methods characteristic of a full size module.

The development activity has indicated that this deployable modular approach toward building large structures in space will support erection of 450 m apertures for operation up to 3 GHz with a single Space Shuttle Flight. Multiple launches will provide unlimited aperture size capability to the limit of efficiency dictated by the use and maturity of full space

erection or space fabrication techniques. The modular concept is compatible with the incorporation of secondary structure for the reflecting surface as well as active surface control systems. Addition of these elements provides the potential for operation of these large structures in the mm wave region.

Use of trade names of manufacturers in this report does not constitute an official endorsement of such products or manufacturers, either expressed or implied, by the National Aeronautics and Space Administration.

2.0 MODULE DESIGN DESCRIPTION

2.1 Module Structural Arrangement

The general arrangement of the modular concept is shown in Figure 1. Each module is made up of small diameter (1.27 cm), thin wall (.4 mm) tubes which are hinged so as to stow as a cylindrical package approximately 25 cm in diameter by a length of about 5/8 the diameter of the deployed modular segment. The module deploys into a space frame structure with a truss supported hexagonal reflective mesh front surface and a triangular rear support frame connected to the front surface by cross braces. Each module is of a depth equal to .86 times the diameter across the corners of the hexagon.

Figure 2 shows the demonstration model at several points in the deployment sequence. Deployment is achieved by operating a jackscrew mechanism located at the center of the module which separates the center pivots of the two sets of radial arms in the upper surface truss. During this motion the arms rotate outward and downward to deploy the surface. The perimeter arms, which are hinged at the center and folded parallel to the upper radial arms in the stowed position, are allowed to deploy by the deploying radial arms. The deployment energy for the perimeter arms is obtained from springs within the center fold joint, as seen in Figure 3. When the arm reaches its fully deployed position (straight), this spring activates a latch locking the arm into the open position. Thus the six perimeter arms form, when deployed, a rigid hexagonal outer hoop.

The rotation of the jackscrew shaft also pays out cables from drums which allow the cross braces and lower structure to deploy. The deployment forces for deployment of these members are supplied by spring loaded joints located at the mid-span fold joints of each set of cross braces

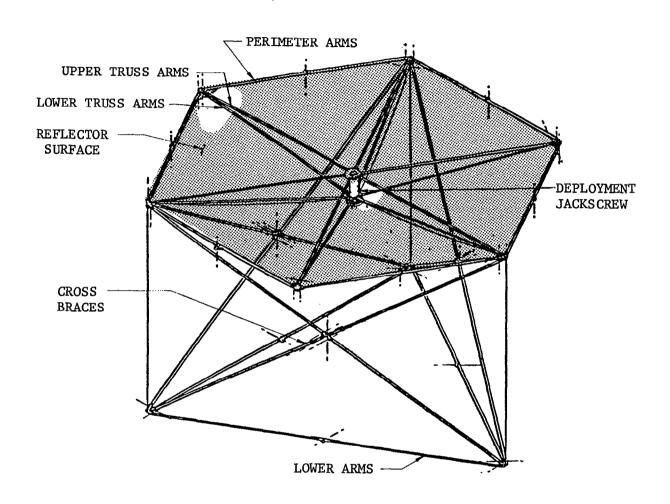


Figure 1. General Arrangement, Deployable Module.

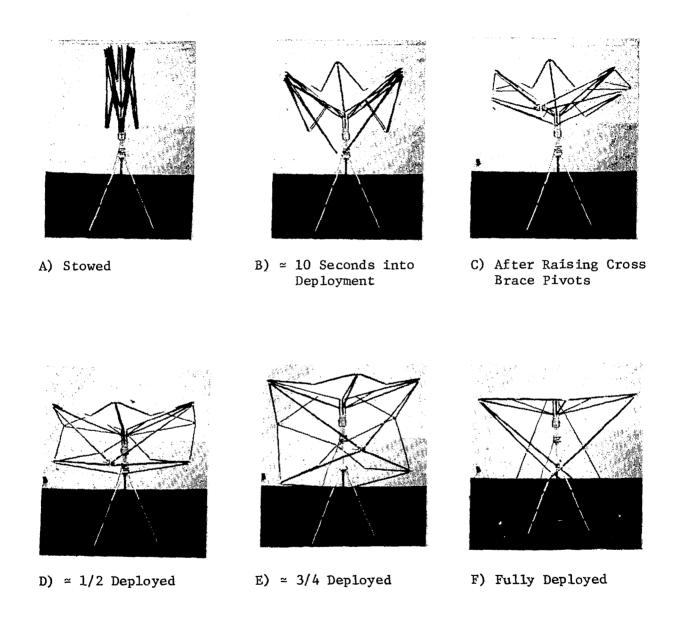
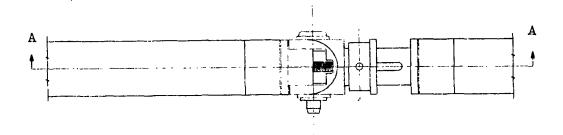


Figure 2. Deployment Sequence - Demonstration Model.



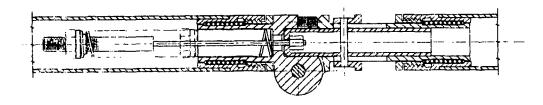


Figure 3. Center Fold Joint, Perimeter Arm.

5

and the center fold joint of each bottom frame member. Each of these springs also operates a latch to lock the joint in its fully deployed position. The cable spool pays out slightly more cable than required for the deployment motion to insure that there is no residual cable tension in the deployed module.

2.2 Kinematic Description

2.2.1 Front Surface Description. The front, or reflective surface support, face of the module is made up of six equally spaced radial four bar linkages and an outer perimeter ring made up of six singly folded arms. Figure 4 displays the kinematic motion for one of the radial linkages. As can be seen, the motion of each of these links is straightforward. Figure 5 depicts the motions of one of the perimeter arms and Figure 6 details the torsional rotation requirements of the mid-beam joint. It can be seen from the diagram that the links must accommodate 60° of relative pivot axis rotation during deployment. Furthermore, since the pivot axes of joints B and C of Figure 6 must be normal to the centerlines of the links (in order for them to stow parallel), and the mid-beam pivot must remain in a radial plane, there is only one stress free kinematic solution. The end pivot axes are chosen parallel to each other and the mid-beam pivot and torsional joint are incorporated into each link at the mid-joint to allow the required torsional freedom. Using this configuration allows a minimum stowed radius (since the tubes can be arranged essentially in a circle) allows the beam end fittings to be identical to those used at the inboard end of the upper and lower radial arms, and allows the centerlines of the deployed perimeter arms, upper radial arms, and lower radial arms to intersect at single points located at each of the six corners of the deployed hexagonal surface, providing for direct, axial load paths in the beams.

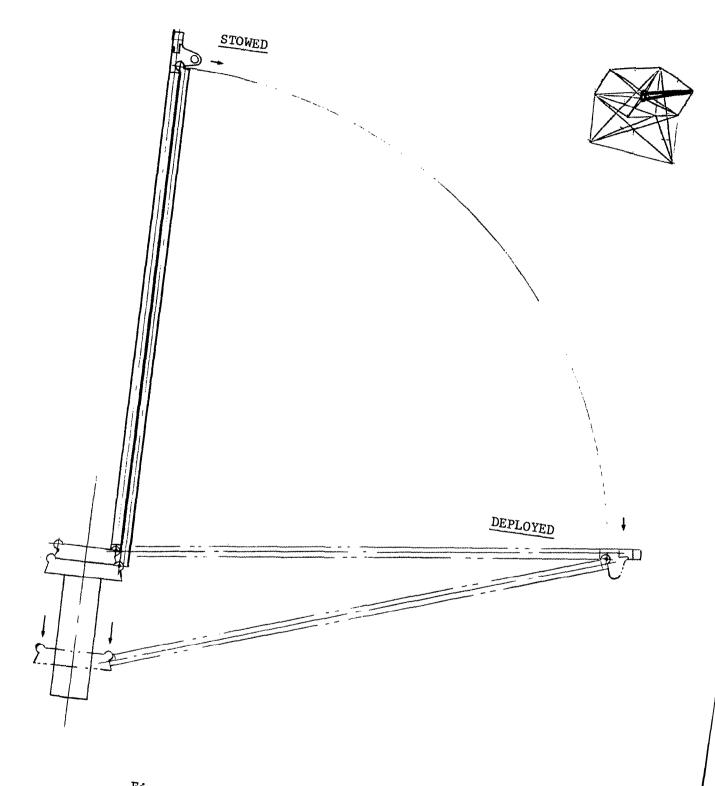


Figure 4. Front Surface Linkage Kinematics.

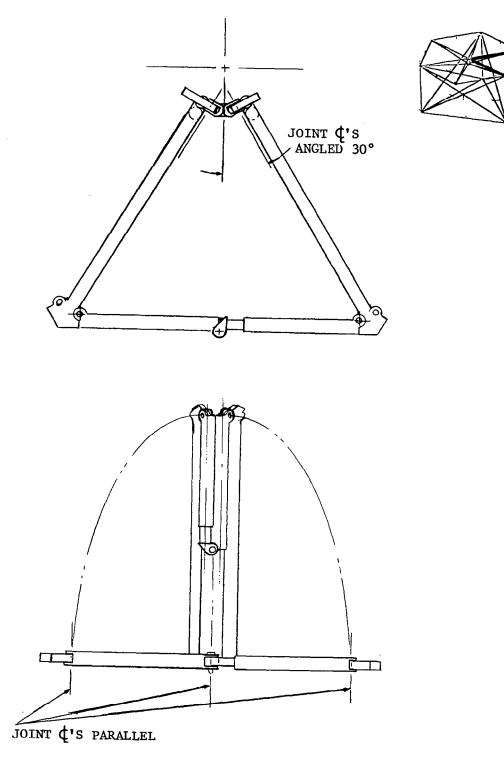
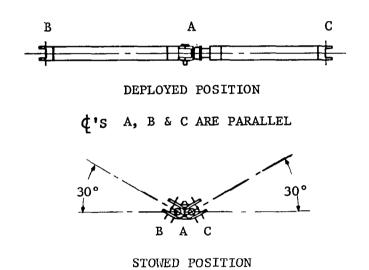


Figure 5. Perimeter Arm Deployment Kinematics.





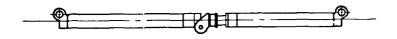
↓ S B & C HAVE EACH ROTATED 30° WITH RESPECT TO A

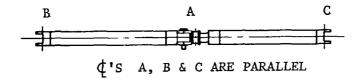
Figure 6. Perimeter Arm Mid Joint Kinematics (Torsional Rotation).

- 2.2.2 <u>Lower Structure Description</u>. Figure 7 describes the joint motions of the lower arms. The kinematic requirements can be seen to be similar to the perimeter arms, differing only in that the total rotation requirement is 120° rather than 60°.
- 2.2.3 Intermediate Structure Description. The remaining kinematic motions are those of the connecting cross braces between the upper surface and the lower structure. Figure 8 shows the deployment motion of one set of these cross braces. As can be seen, the motions of each brace are complex curves; they require, however, only Cardin joint motions (i.e., pivot motions about two perpendicular axes, both perpendicular to the link centerlines; similar to a common universal joint) at each end plus torsional rotation of one end of the beam with respect to the other. Two kinematic solutions to the problem are possible at the center cross joint (see Figure 9), i.e., the joint can be arranged with the central pivot axis either vertical or horizontal. With the pixot axis vertical, Figure 9A, the torsional motion required during deployment is approximately 135°, occuring at the end of deployment. If the center pivot is aligned horizontally, Figure 9B, the torsional motion requirement decreases to a maximum of approximately 45° occurring during deployment and decreasing to near zero at full deployment. However, the Cardin joint travels for this case are such that during deployment the center beam pivot must travel past its position at full deployment. Therefore, in order to use this arrangement, the travel stop which currently prevents the brace from rotating past its fully deployed position would have to be replaced by some sort of detent arrangement. This requirement would complicate the joint design unnecessarily. Therefore the configuration shown in Figure 9B was chosen for the mechanism.

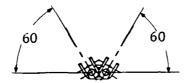
2.3 Demonstration Model Description

DEPLOYED POSITION



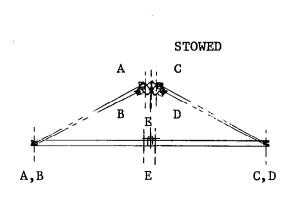


STOWED POSITION

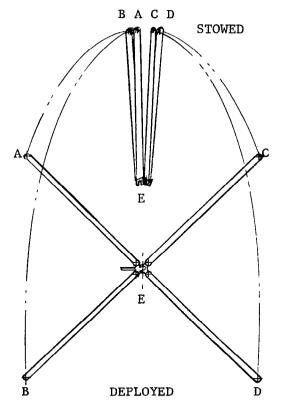


Q'S B & C HAVE EACH ROTATED 60° WITH RESPECT TO A

Figure 7. Lower Arm Kinematics.







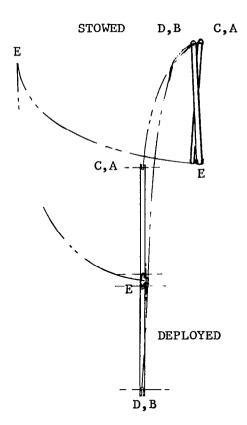


Figure 8. Cross Brace Kinematics.

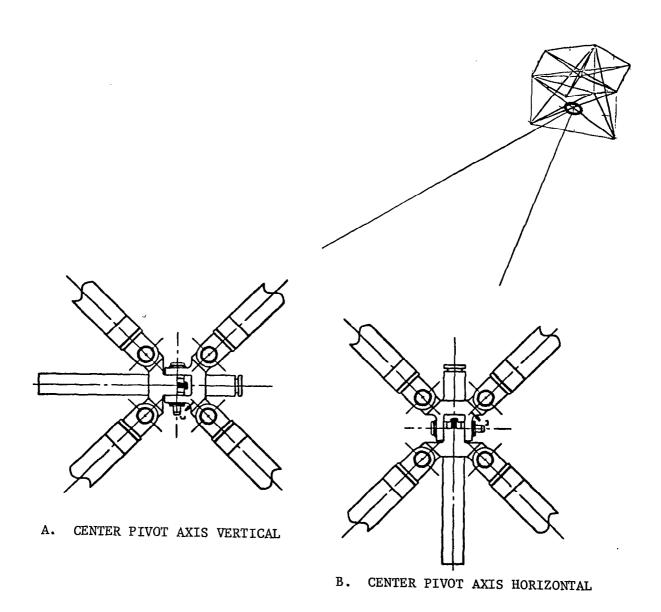


Figure 9. Cross Brace Center Joint Configuration.

2.3.1 Requirements and General Arrangement. The foregoing kinematic study and module tube sizing (Sections 2.2 and 2.1) established a number of design requirements for a demonstration model of the deployable module. Table I gives the full list of design requirements for the assembly. Figure 10 shows the model in its stowed position, Figure 11 shows it fully deployed, and Figure 12 lists pertinent features and overall dimensions of the structural members. The 1.57 m (62 in.) dimension across the corners of the hexagonal surface is chosen to make the overall height of the stowed module/deployment stand assembly approximately 2.25 meters, allowing the model to operate satisfactorily in a room with an 2.4 m (8 ft.) ceiling. The material selected for all the strut members is 1.27 cm (.50 in.) OD x .7 mm (.028 in.) wall fiberglass tubing per NGMA G commercial specification. This tubing is readily available in .8 m (32 in.) lengths, and therefore can be used in single lengths for all struts except the diagonal cross braces, which must be spliced.

The reflective mesh used on the model is a Dacron woven mesh, identical to the mesh used on the ATS-6 reflector in 1974. The mesh is sewn to the upper radial struts with Dacron thread. The thread is routed through brass eyelets in the tubing to prevent chafing during deployment motions.

The model is deployed by an electric motor operating through reduction gearing, driving a jackscrew located at the center of the radial arms. The motor and gearbox are housed at the top of the removable deployment/display stand (see Figure 10). This component arrangement allows one deployment motor assembly to deploy any number of reflector modules, which can then be released from the deployment motor unit and assembled into a completed structure. The display stand itself is a folding tripod, which has been modified to mount the motor/gearbox and support the model at the correct height for ground clearance at full deployment.

¹Dacron: Registered trademark of E. I. du Pont de Nemours & Co., Inc.

TABLE I DEMONSTRATION MODEL DESIGN REQUIREMENTS

- Model to be driven for "hands off" deployment.
- Model to be deployable in a room with an 2.4 m (8 ft.) ceiling.
- Model tube size to be 1.27 cm (.5 in.) diameter.
- Joint fittings shall be aluminum.
- Stowed package diameter shall be minimized.
- Model shall be equipped with a reflective surface material,
 which shall be attached to the upper structure to form a flat faceted, hexagonal surface.

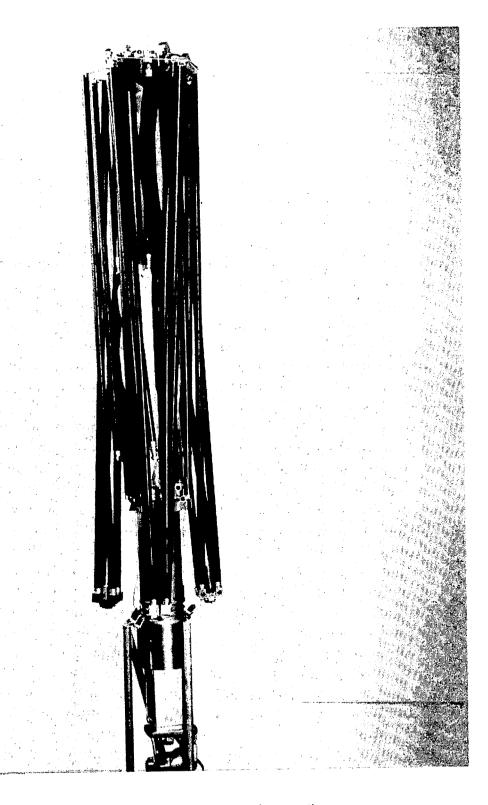


Figure 10. Demonstration Model (Stowed)

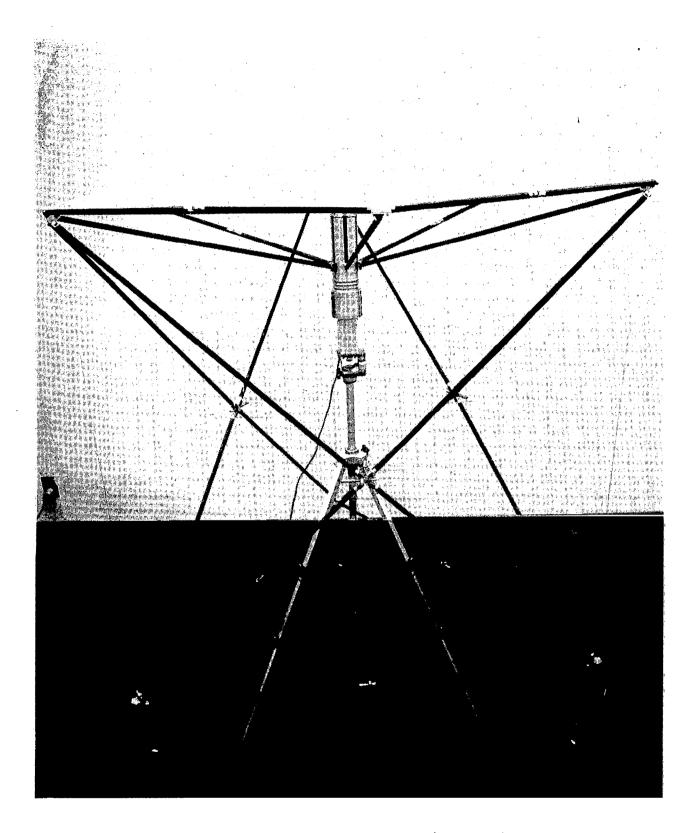


Figure 11. Demonstration Model (Deployed)

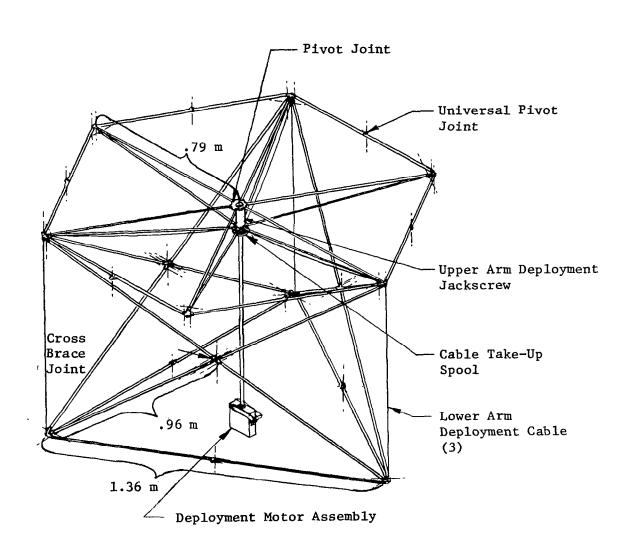


Figure 12. Demonstration Model Assembly.

2.3.2 <u>Deployment Mechanism</u>. Figure 13 shows a closeup of the deployment jackscrew mechanism in the stowed position, and Figure 14 shows a cross section of the mechanism. To deploy the module, the electric motor rotates the cable spool and shaft. This rotation forces the slider to move axially along the outer tube, thus moving the inboard pivots of the six lower radial arms downward. The upper radial arms are rotated outward about these inboard pivots by the lower arms.

The deployment synchronization cable spool is attached to and rotates integrally with the screw shaft. In the stowed position the spool stores the three .80 mm diameter stainless steel cables which are used to control the deployment rate of the truss braces and lower struts. As the shaft is rotated, these cables are payed out, allowing the spring loaded joints to deploy the lower structure.

2.3.3 <u>Joint Description</u>. The module's structural elements are connected by pivoting joints to allow for stowage. While there are a total of 54 joints in the module structure, they break down into 4 basic different types. There are 36 single axis clevis joints, of the type characterized by the inboard radial arm pivots, Figure 12. Figure 15 indicates the locations of these joints, and Figures 16 through 18 are photographs of the individual joint installations in the model.

The second basic joint type is a latching pivot joint plus torsional rotation joint (Figure 19). These joints are required in the model to accommodate the kinematic motions at the perimeter arm and lower arm midspan fold joints. The link lengths in the demonstration model, approximately .4 m for the perimeter arms and approximately .7 m for the lower struts, will not accommodate the 30° or 60° torsion movement required during deployment without structural failure, so this joint includes a torsional bushing on either side of the pivot joint. The joint also incorporates a latch in the center to guarantee structural rigidity in the deployed position. Nine of these joints are used in the model,

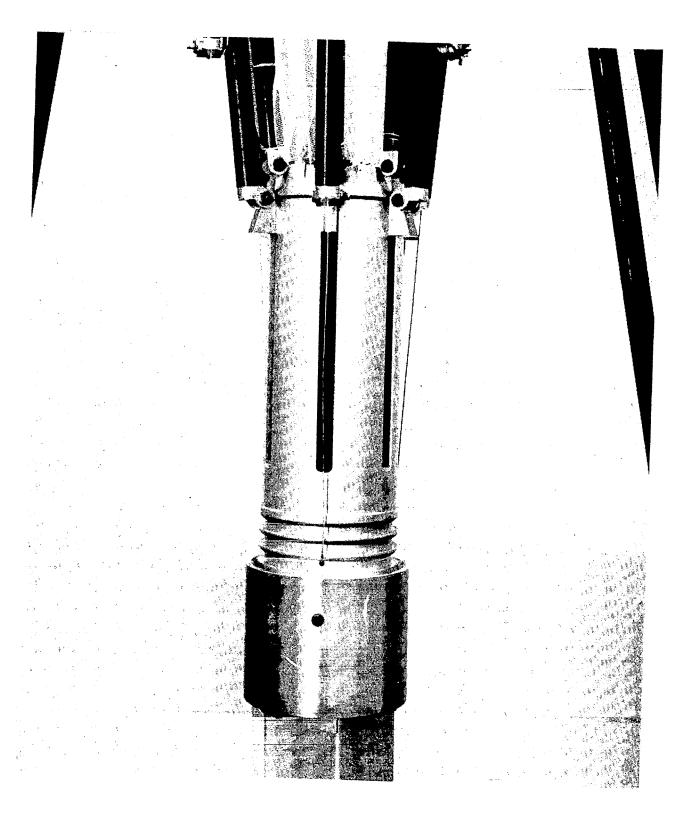


Figure 13. Jackscrew Mechanism (Stowed)

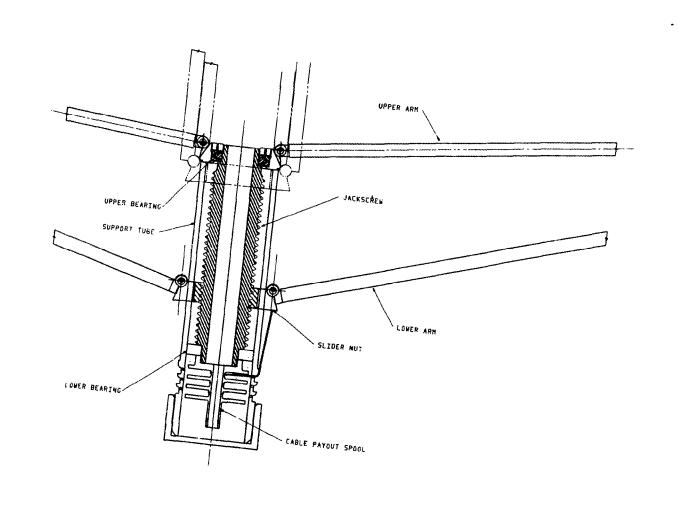


Figure 14. Jackscrew Mechanism (Cross Section).

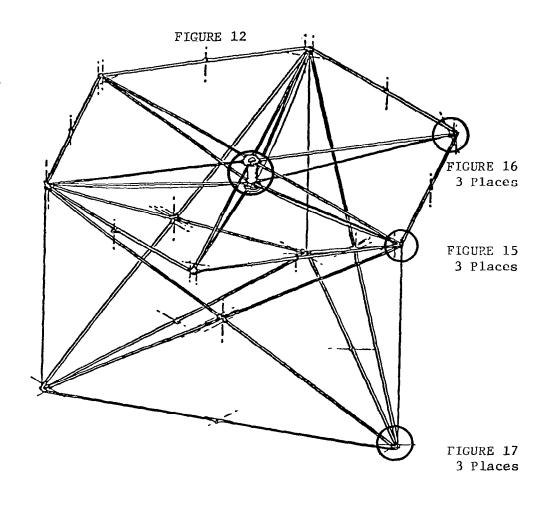


Figure 15. Pivot Joint Location Overview.

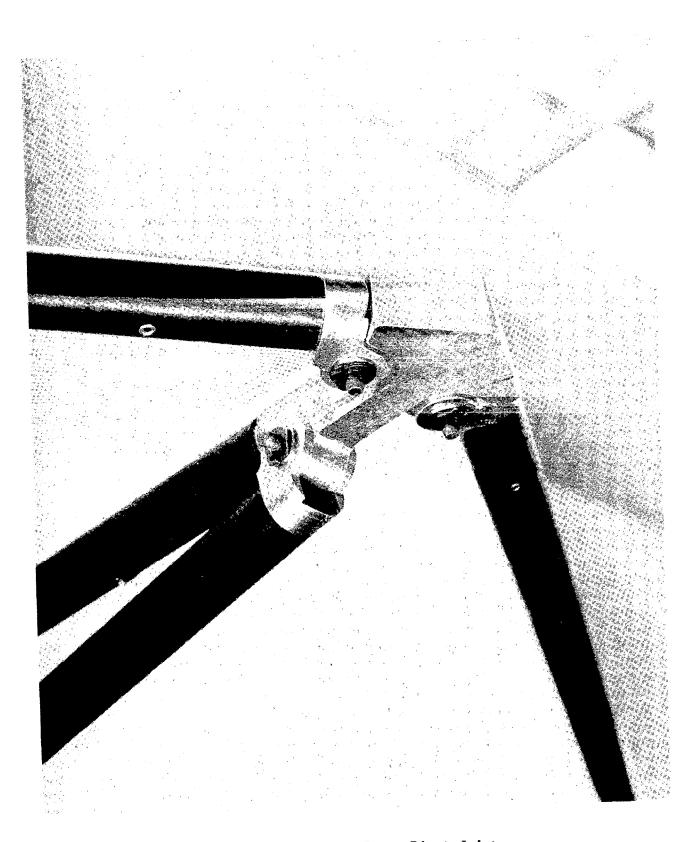


Figure 16. Perimeter Strut Pivot Joints

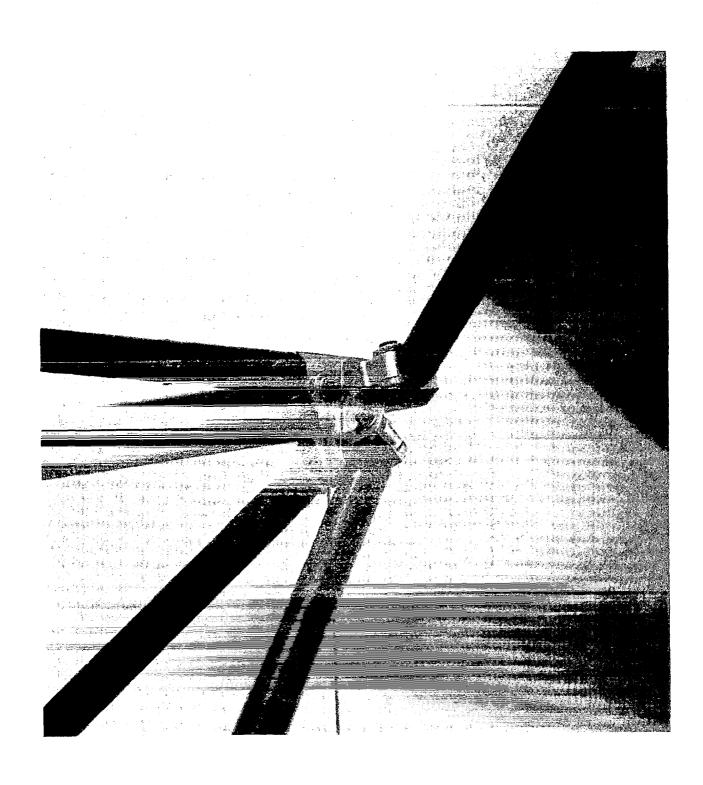


Figure 17. Perimeter Strut Pivot Joints

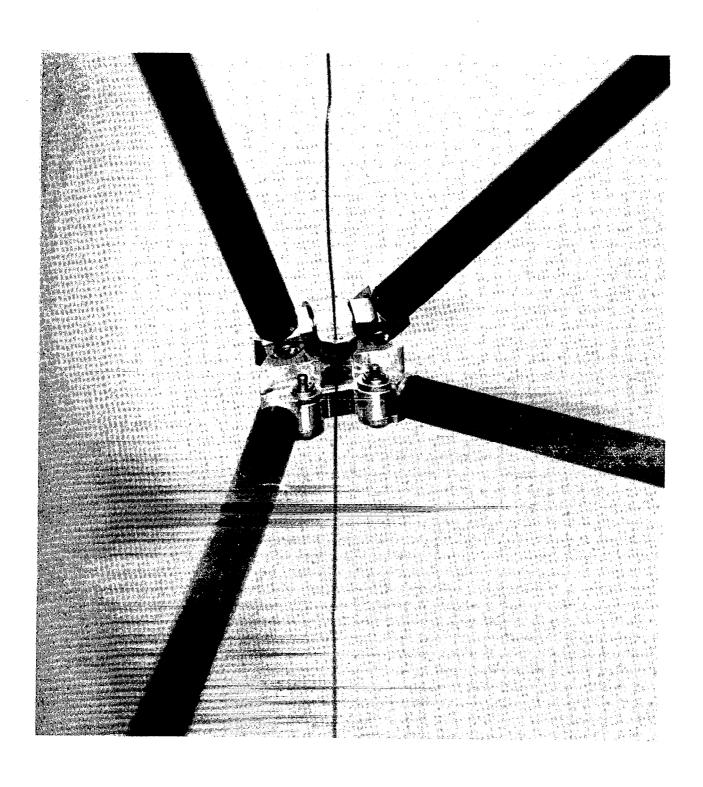
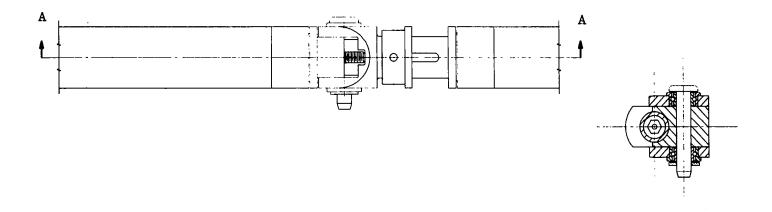
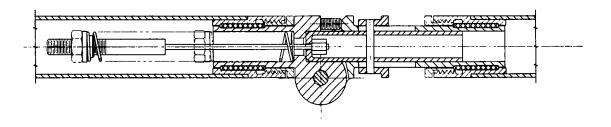


Figure 18. Lower Strut Pivot Joints





SECTION B-B



SECTION A-A

Figure 19. Pivot Plus Torsion Joint.

placed as shown in Figure 20. Figures 21 and 22 are photographs of one of the perimeter arm joints in the stowed and deployed positions.

The deployment motions of the upper and lower ends of the cross braces are accommodated by the third basic joint type in the model, which is a modified Cardin joint. Six of these joints are used in the model, placed as shown in Figure 23 and pictured in Figures 24 and 25. Figure 26 shows a cross section of the upper corner joint. The outboard pivot axis strut fittings are simple clevises identical to the ones used at the inboard end of the upper radial arms. The inboard pivot axis is directed perpendicular to the upper arm fittings and pivots on bearings in the upper arm fitting. This pivot arrangement allows two arm joints to share one set of mounting bearings, and also permits the motion of the inboard pivots of these joints to be slaved together by indexing the shafts of the pivots. This slaved motion forces all of the cross braces to rotate through approximately equal angles during all phases of the deployment motion.

The lower cross brace joints are identical in function to the upper joints, differing only in that, since the inboard pivot axes are further apart, an indexing spacer is inserted between the pivots to coordinate their motions, as shown in Figure 27.

The fourth joint type, shown in Figure 28, is the latching joint connecting the center ends of the cross braces. Three of these joints are used in the module, one at each of the intersections of the sets of cross brace struts.

Figures 29 through 31 are photographs of one of the completed joints in the stowed and deployed positions. This joint combines two sets of dual Cardin joints, torsion bearings in the end of each strut, and spring powered deployment and latching about the center pivot. In addition, travel stops are provided for the outer pivots to prevent travel beyond their fully deployed positions.

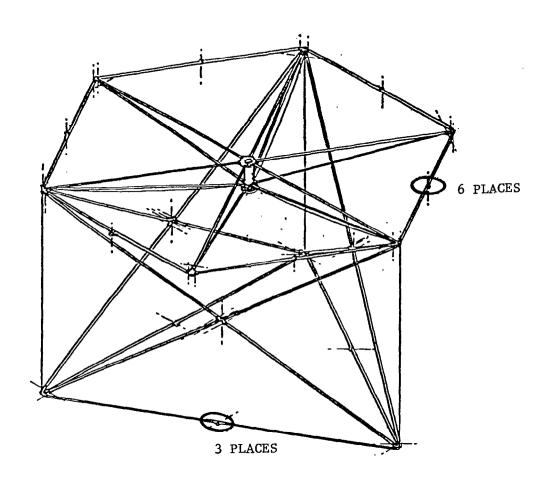


Figure 20. Torsional Pivot Joint Location Overview.

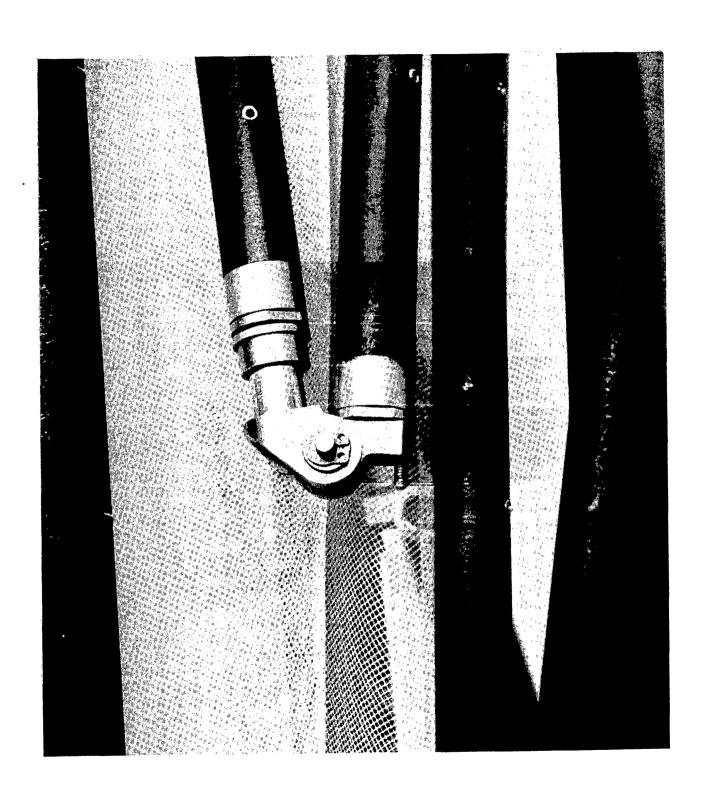


Figure 21. Perimeter Arm Mid-Span Joint (Stowed)

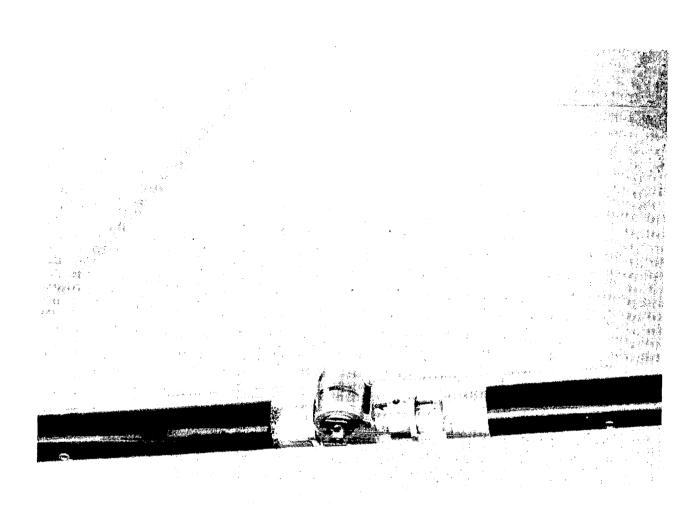


Figure 22. Perimeter Arm Mid-Span Joint (Deployed)

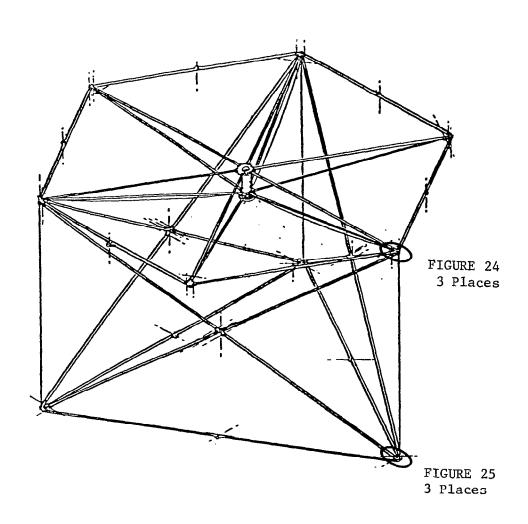


Figure 23. Cardin Joint Location Overview.



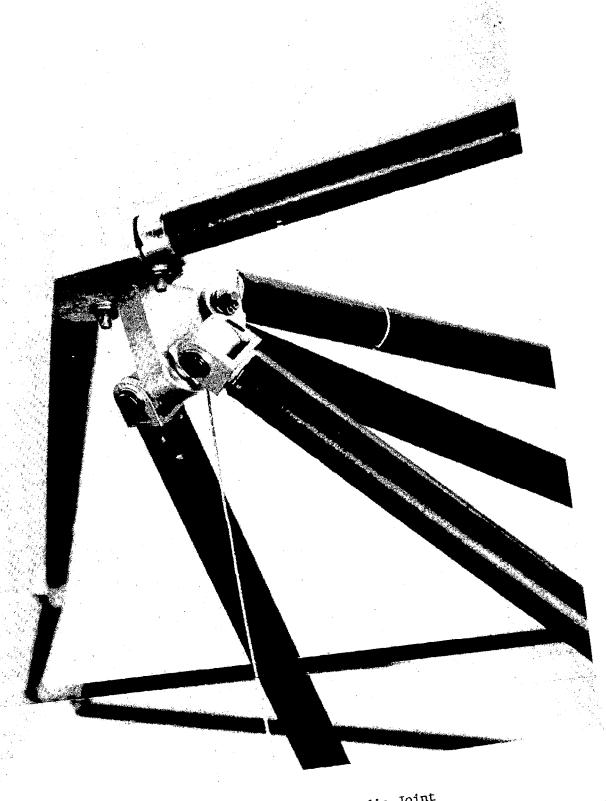


Figure 24. Upper Corner Cardin Joint

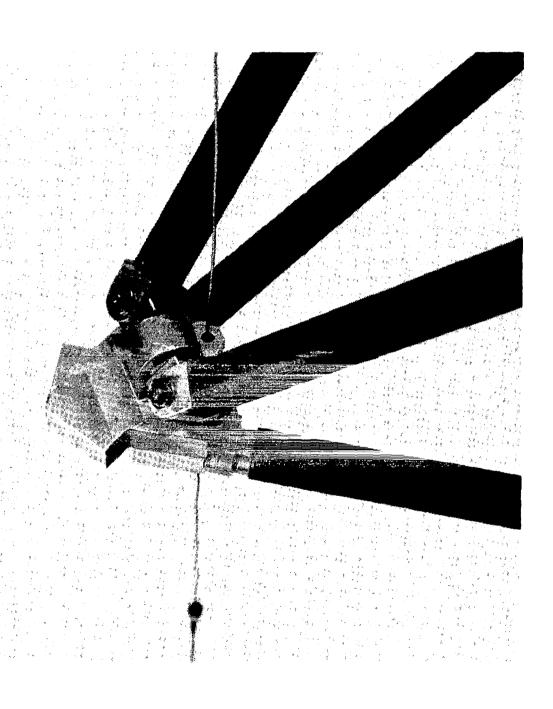


Figure 25. Lower Corner Cardin Joint

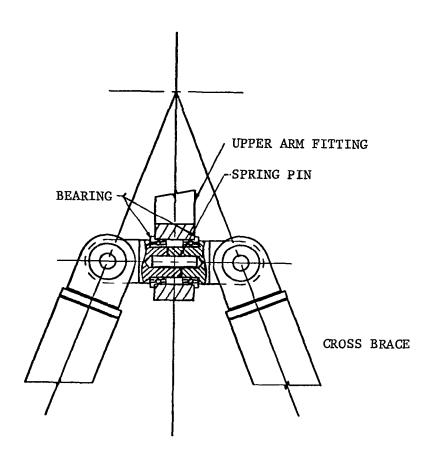


Figure 26. Cross Brace Upper Corner Joint.

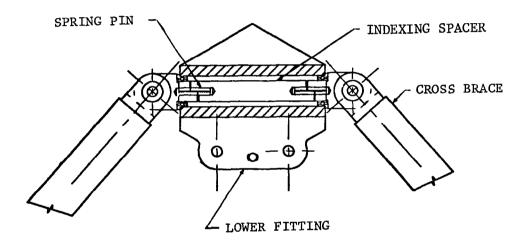
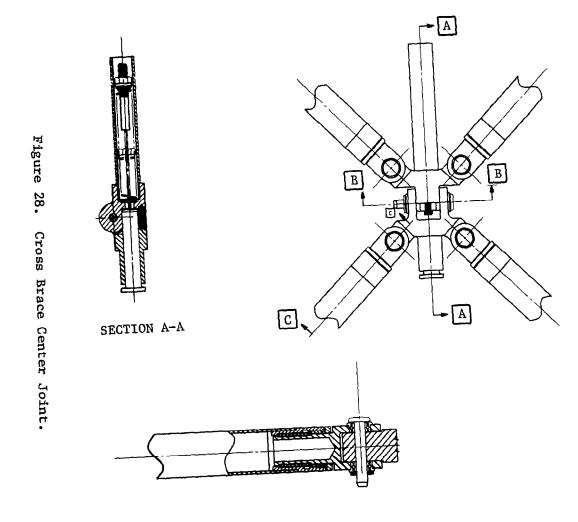


Figure 27. Cross Brace Lower Corner Joint.



SECTION B-B

SECTION C-C TYP 4 PLACES

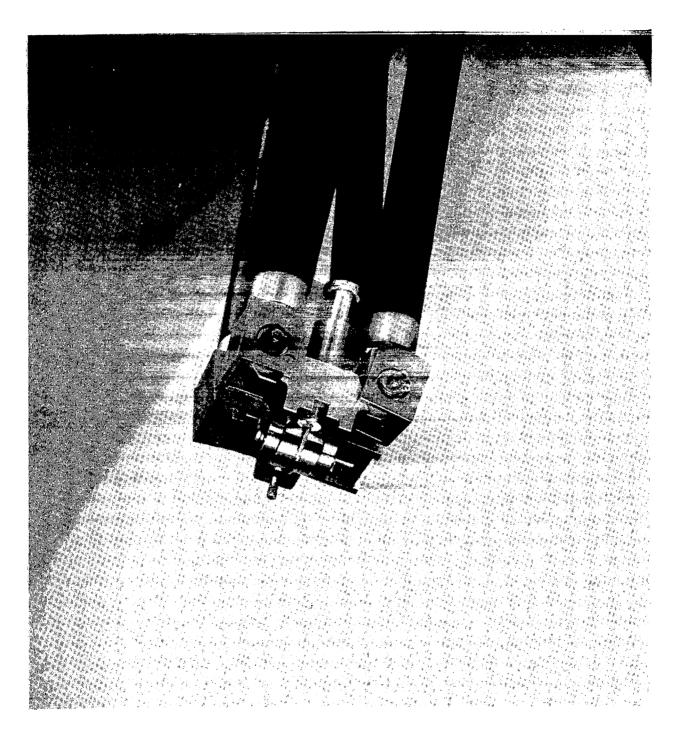


Figure 29. Cross Brace Center Joint (Stowed)

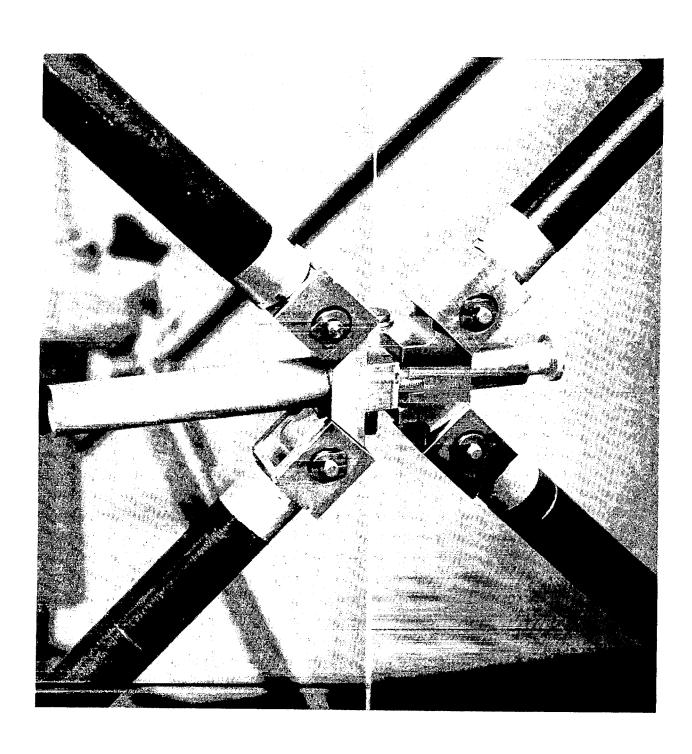


Figure 30. Cross Brace Center Joint (Deployed - Viewed from Outside of Module)

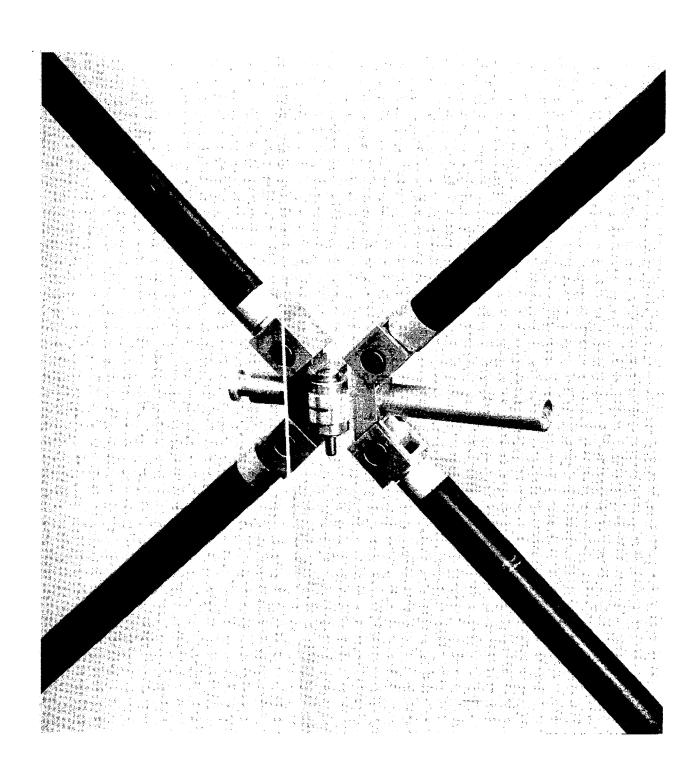


Figure 31. Cross Brace Center Joint (Deployed - Viewed from Inside of Module)

2.3.4 Operation Sequence. The model is designed for transport and demonstration by one man. The model, its support stand, and motor control box are all transportable in one carrying case. The only requirements for the demonstration area are a 2 meter (6.5 foot) diameter area with a 2.25 meter (8 foot) high ceiling minimum and availability of standard 110 volt, 60 cycle electric power.

In operation, once the model is set up on the deployment/display stand, module deployment can be controlled from the motor control box with one pause for zero-gravity simulation. The deployment cycle can then be reinitiated and will continue to completion hands off. The motor control circuit includes, in the deploy direction, a sensing circuit which shuts off power to the motor at full deployment, should the operator be otherwise occupied.

In the retract mode, two switches must be closed to operate the motor. This feature is incorporated to avoid having personnel unfamiliar with the unit attempting to retract the module without installing the hinge latch retention clips. Retraction of the module with the hinges latched will result in structural failure of the tubes, and therefore must be positively avoided.

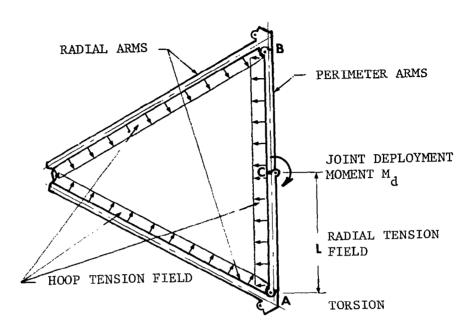
After the unit has been completely retracted, one man can easily return the module to its shipping container.

2.3.5 <u>Demonstration Model Performance</u>. The initial assembly and deployments of the model validated the kinematic models and identified several areas for improvement. These results and their implications on antenna module design are discussed in the following paragraphs.

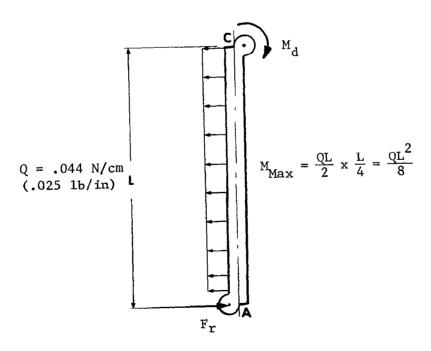
Surface Considerations

The initial configuration of the model included a knitted metal mesh as the reflective surface. This mesh was sewn to the upper radial arms and perimeter arms to hold it in place. The mesh surface was prepared, and tacked to the model. Initial deployment attempts were made and the mesh was found to prevent the perimeter arms from fully deploying and latching. The difficulty was traced to the requirement, in knitted meshes, for maintaining the mesh in a biaxial tension field to eliminate edge curling, wrinkling, and to maintain the design knitted cell size. Figure 32 presents the boundary forces which must be reacted in a typical panel of the model. The particular mesh chosen required a radial tension of approximately .044 N/cm (.025 lb/in.) resulted in a deployment resisting moment about point C of approximately .5 N-m (5 in.-1b). The moment about the joint from the hinge spring at this point is approximately .24 N-m (2.1 in.-1b), coming from the 36.5 Newton (8.2 lb) force remaining in the spring at this point in the deployment motion. The arm then would require a 90 Newton (20 1b) axial load in the hinge spring, in order to insure full deployment. This spring force would be excessive when extrapolated to a full scale mode. A graphite/epoxy tube with a 1.27 cm 0.D. and .7 mm wall thickness and a material bending stress allowable of 689,500 KPa (100,000 psi) has an allowable tube bending moment of approximately 16.9 N-m (150 in.-1b). With the tension field as shown in Figure 32B, this graphite epoxy tube will fail due to the tension field at a length of 5.5 meters. This would limit the modules to sizes of less than 11 meters across the corners. As a result of this concern, design solutions were identified and reviewed. The mesh radial tension load restriction can be removed by using a woven rather than knitted mesh. The woven mesh configuration derives the required shape restraint from loads only in the circumferential threads. In the interest of continuing the experimentation, the mesh on the model was changed to a woven Dacron identical to that used on the ATS-6 reflector. Since the woven mesh need only be attached to the radial arms, the adverse loading on the perimeter arms and hinges the deployment problem was eliminated.





A. MESH TENSION FIELD IN MODEL.



B. TENSION FIELD ON PERIMETER ARM.

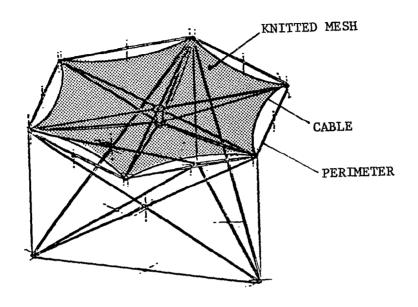
Figure 32. Knitted Mesh Free Body Diagram.

A second solution to the knitted mesh problem can be obtained by connecting cables between the tips of each upper radial arm. The knitted mesh would then be attached to the circumferential cable as shown in Figure 33. Therefore, the mesh loads would all be reacted by the radial arms, and the perimeter arms would be free to deploy independently. This solution would, however, result in non-reflective gaps in the reflective surface of the assembled reflector due to the catenary shape of the mesh loaded cables around the perimeter of each module hexagon.

Kinematic Considerations

During assembly, an interference was noted between the upper and lower cross brace arms in the stowed position. The interference forced the lower ends of the arms radially outward and prevented them from stowing parallel to the centerline of the model. The "veeing out" of these arms is shown in Figure 34, and the arrows on the figure denote the area of interference. Experimentation with the lower corner pivot points disclosed that the problem could be eliminated by moving the lower cross brace corner pivots outward approximately 1.5 cm and downward 2.25 cm. New lower corner fittings were manufactured to relocate the pivot points, and the struts then folded in neatly along the sides of the unit, reducing the stowed diameter from approximately 36 cm to approximately 25 cm.

The model also exhibited excessive torsional free play motion in the deployed position. This motion was traced to axial and torsional manufacturing tolerances in the torsional joints. This is of little consequence for a full scale module since graphite/epoxy tubes in lengths exceeding 7.25 meters (corresponding to module sizes of approximately 12 m or larger across the corners of the hexagonal surface) can absorb the required torsional motion as elastic torsional bending in the stowed configurations. This eliminates the need for these discrete torsion joints.



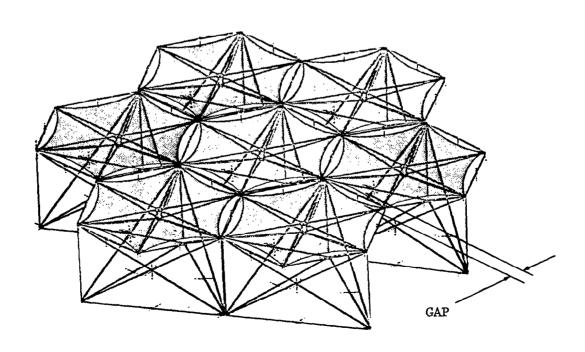


Figure 33. Knitted Mesh Module Configuration.

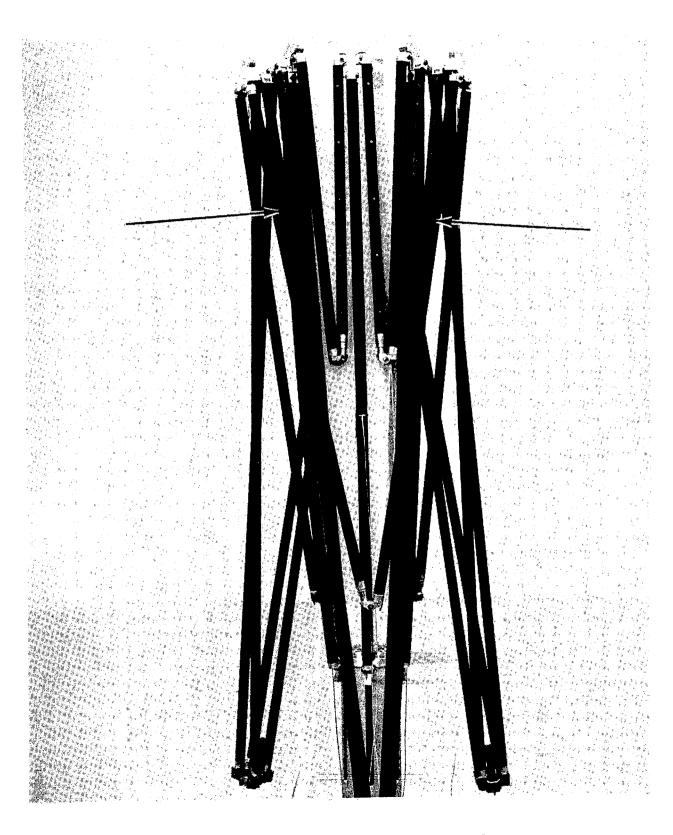


Figure 34. Stowed Model Showing Tube Interference

W

Initial deployments of the model also verified that in the early phase of deployment, the cross brace kinematics are such that each set of four arms must rotate about the upper joints for approximately 85 degrees (very nearly horizontal) before the lower arm corner fittings separate significantly from the upper joints. During this phase, or approximately the first 10 seconds of deployment, the weight of the links is such that the model's normal deployment forces are unable to rotate them against gravity, resulting in the arms hanging downward forcing the lower corner fittings up against the upper corner fittings as shown in Figure 35. Deployment must be interrupted at that point and the cross braces raised by hand against gravity to allow the lower corner fittings to deploy. Figure 36 shows the model after this operation. This action also required some means to control the cables being released from their storage spools to prevent tangling or binding. As an initial control, weights were used to provide a constant tension load on the cables, but were later replaced by adding spring loaded service loops to the cable runs. These service loops in the cables also served to eliminate variations in cable length due to uneven cable winding. The actual cable required on the spools was approximately 33 cm more than calculated for smooth winding and winding path differences caused length variations of + 1 cm from deployment to deployment. This variation indicates the need, on full scale units, to either control the cable with winding guides similar to those used on fishing reels, or to use other flexible members (such as tapes) as substitutes for the cable whose spooling can be more exactly determined and controlled.

The final model limitation discovered was that the lower arms which form the folding lower truss members were unable to fully deploy against the force of gravity. The moment about the deployment hinge due to the weight of the arms in the horizontal position overpowers the deployment moment in the spring loaded hinge. This was overcome in the model by using a cord between each lower arm folded joint and its corresponding lower radial arm. As the model nears full deployment, these cords become

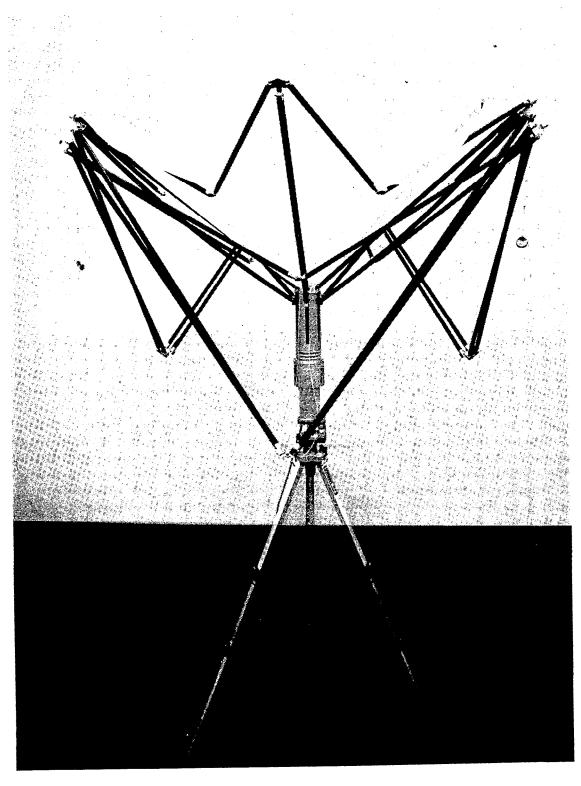


Figure 35. Partially Deployed Model (Cross Brace Deployment Hindered by Gravity)

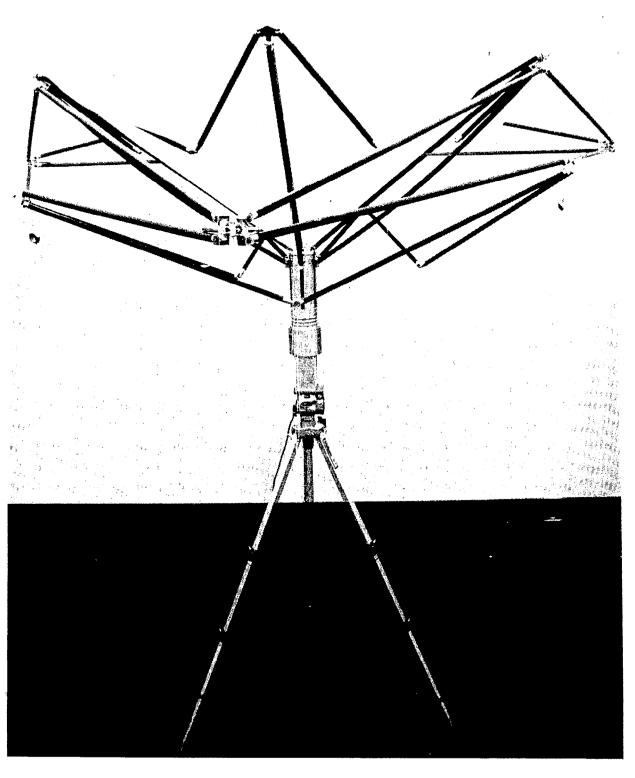


Figure 36. Partially Deployed Model (Cross Brace Raised to Allow Lower Arm Deployment).

taunt, relieving the weight from the arm allowing the spring loaded joint to deploy fully and latch.

The 1 g deployment difficulties encountered with the model are indicative of a class of problem which must be addressed during construction and test of full scale modules. Very light weight structures of this type are not capable of supporting themselves in a 1 g Earth environment. Construction of full scale modules will have to be performed in assembly structures which will support the members in undeflected quasi-zero g positions. This support will have to be maintained during stowage operations on the modules, and during any deployment testing. Thus it may well come to pass that structures of this size will be subjected to component testing only and that the initial deployment of the complete structure will be performed in orbit.

2.3.6 <u>Model Weight Description</u>. The Demonstration Model components were weighed after assembly. The component weight breakdown for the assembly is given in Table II. The weight of the deployment mechanism is not representative of flight hardware, and could be reduced by approximately 40%. If this were done, the total mass of the assembly would reduce to approximately 4.45 kg, and the joint mass fraction would be approximately 28%.

2.4 Full Scale Module Description

2.4.1 General Arrangement and Scaling Parameters. Applications for space antennas through the next decades point to requirements for very large (.5 - 1 km diameter) apertures operating at gigahertz frequencies. In order to launch such antennas economically, efficient methods for packaging these reflectors into the STS Orbiter cargo bay for launch are essential. The modular antenna concept shows significant promise for this application.

TABLE II DEMONSTRATION MODEL WEIGHT BREAKDOWN

| COMPONENT | NO. USED | MASS (WI kg (LE | ** | (WT) (LB) |
|---------------------------------|----------|--------------------|---------|--------------|
| CENTRAL DEPLOYMENT MECHANISM | 1 | 2.4 (5.2 | 25) 2.4 | (5.25) |
| UPPER CORNER FITTING (6 ARM) | 3 | .04 (.0 | .12 | (. 27) |
| UPPER CORNER FITTING (4 ARM) | 3 | .035 (.0 | .11 | (.24) |
| LOWER CORNER FITTING | 3 | .05 (.1 | .16 | (.36) |
| MID BEAM PIVOT HINGE | 9 | .03 (.0 | .27 | (.66) |
| CROSS BRACE CENTER HINGE | 3 | .05 (.1 | .15 | (.33) |
| UPPER RADIAL ARMS | 6 | .04 (.0 | .23 | (.51) |
| LOWER RADIAL ARMS | 6 | .04 (.0 | .24 | (.53) |
| PERIMETER ARMS | 12 | .02 (.0 | .25 | (.55) |
| LOWER STRUCTURE ARMS | 6 | .04 (.0 | .21 | (.46) |
| CROSS BRACE STRUTS | 12 | .05 (.1 | .57 | (1.25) |
| MESH | 1 | .15 (.3 | .15 | (.34) |
| |] | TOTAL | 4.86 | (10.75) |

The kinematics, joint concepts and deployment mechanism of the modular antenna demonstration model can be scaled directly to Orbiter cargo bay proportions. The only significant change required to produce a full scale antenna model is to increase the length of the individual struts. The useful size of the Orbiter cargo bay, after allowing room for Astronaut ingress/egress to the bay, is a cylinder 4.5 m (15 ft.) in diameter by 17.1 m (56 ft.) long. This limits the module size by constraining struts lengths to 17.1 m cargo bay length. This constraint leads to 28 meters across the corners of the hexagonal face as a maximum practicable module size compatible with STS launch. Figure 37 shows the general arrangement of such a module, and the resulting strut lengths, the longest of which is the 17.1 m (56.25 ft.) cross brace member. Buckling of the struts due to module loads is the only other size limiting parameter. A full load analysis for the module antenna structure was not performed since the design loads are mission peculiar. Such an analysis should be performed when a focus mission is defined.

- 2.4.2 <u>Module Weight Breakdown</u>. The modular antenna concept, in full scale versions, promises very efficient support structures for antenna reflector surfaces. A graph of module mass vs size is given in Figure 38, and component mass fractions vs size are shown in Figure 39. It can be seen that for a 28 m module the mass fraction of the module structure is 20%, increasing to 43% for a 10 meter module. A comparative mass fraction for a previous technology reflector (the ATS-6, 9.1 meter diameter reflector) is 91% structure.
- 2.4.3 Mesh Attachment. The attachment of the reflective mesh to the reflector supporting structure is of prime importance in reducing surface distortions, which in turn cause loss of overall antenna efficiency. Many different methods of securing the mesh to its support structure have been tried, and in general those methods which are simplest in concept, using the least number of differing types of materials, have proven best.

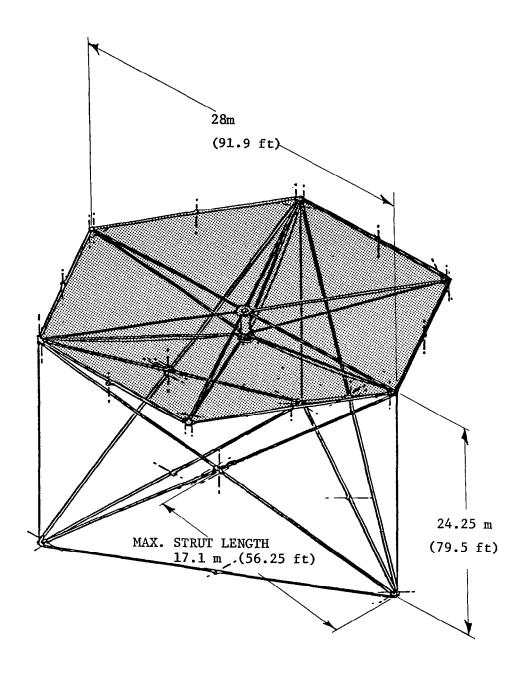


Figure 37. Maximum Size Module for STS Launch.

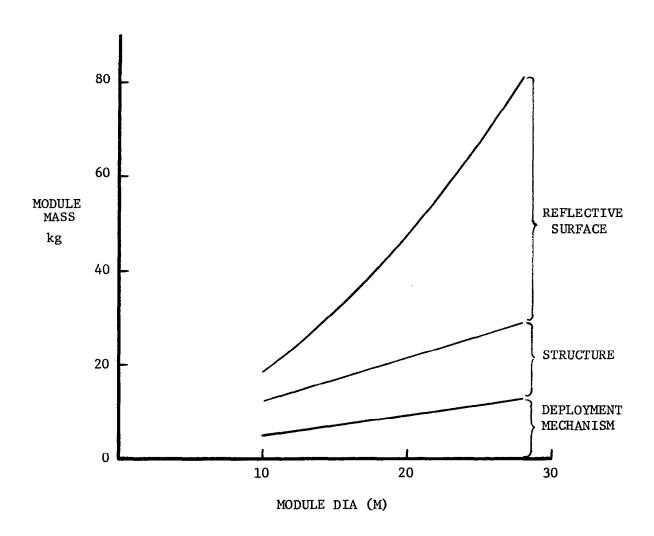


Figure 38. Module Mass vs Size.

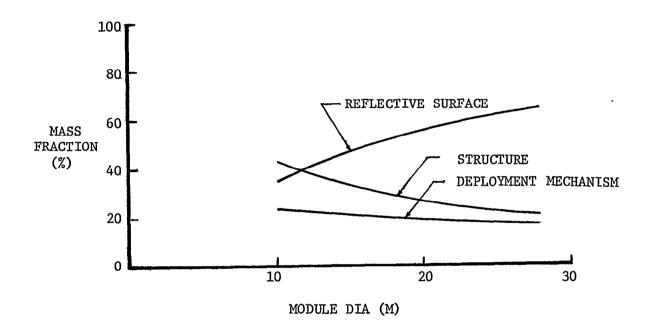
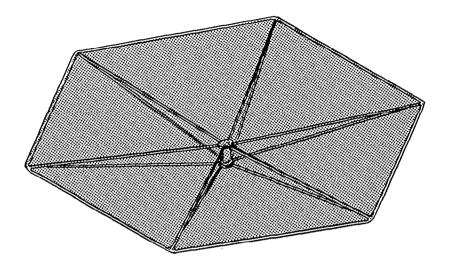


Figure 39. Module Component Mass Fractions vs Module Size.

Figure 40 demonstrates the method of attaching a mesh surface to the tops of the radial tubes. This method was employed on the demonstration model, and works satisfactorily. From the performance studies described in Section 3, it can be seen that higher frequencies of operation may be obtained, due to the closer approximation to a true paraboloid, by providing a curved standoff support for the mesh. Figure 41 describes the attachment method used with this type of support.

Closer approximation to the true paraboloid can also be obtained by using surface augmentation schemes which control the position of the reflective mesh as if the support structure consisted of more elements. Figure 42 describes two such approaches. Figure 42A depicts a reflective surface augmentation scheme using discrete attachment points at the center, mid-points, and ends of each radial arm and at the center of each perimeter arm. The mesh would be constrained along the connecting lines between these points using quartz tension cords. Figure 42B describes a similarly augmented surface but without the complexity of the tie points at the mid-points of the perimeter arms.



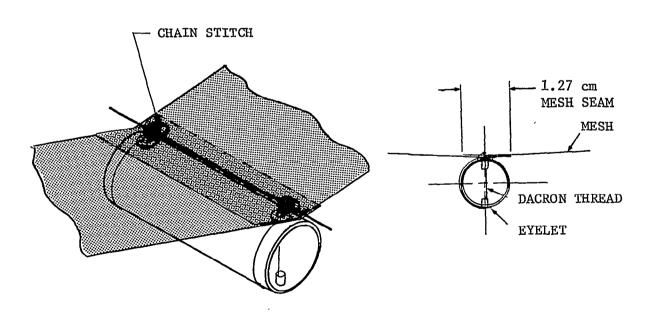
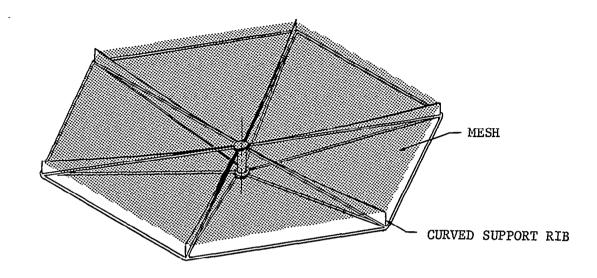


Figure 40. Mesh Attachment to Radial Tubes.



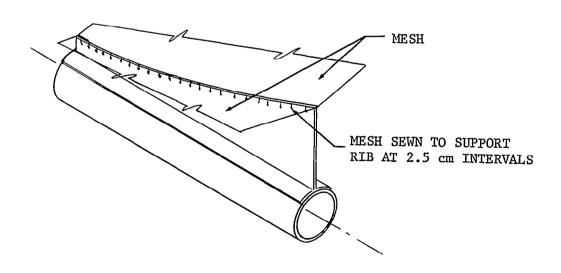
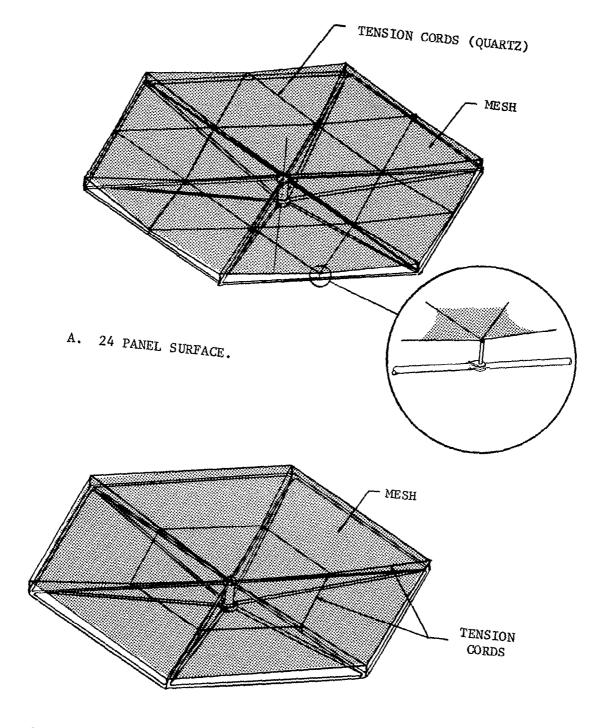


Figure 41. Mesh Attachment to Curved Standoff.



B. 12 PANEL SURFACE.

Figure 42. Surface Augmentation Methods Using Mesh Ties.



3.0 LARGE REFLECTOR STUDIES

3.1 Large Reflector Requirements

Major emphasis in the Aerospace Community is currently being placed on development of extremely large space systems for public benefit.

NASA, specifically Goddard, Langley, and JPL, have announced plans to place parabolic and/or array antennas in space for use in public services, solar power transmission, radio astronomy and communications. These missions identify requirements for reflectors with apertures of up to 1000 meters.

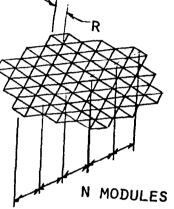
The studies below estimate the radio frequency performance, module deployment, any joining techniques, and reflector assembly procedures applicable to the construction of these large space-borne reflectors.

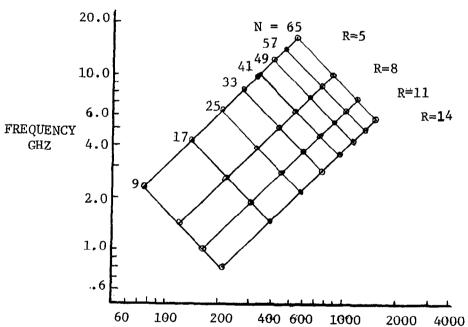
3.2 Reflector Performance Studies

A parametric computer code has been prepared to define the RMS surface deviation for reflectors made up of large numbers of modules. The study used the module diameter, number of modules across the reflector face, and reflector focal length/diameter (f/D) ratio as input variables; and obtained RMS surface deviations as output. For this analysis, the basic six element module approximation (Figure 41) was used. These data are compiled as Appendix B to this report, and the data is graphed in Figures 43 through 46. Note that thermal distortions in the reflector are not included in these charts.



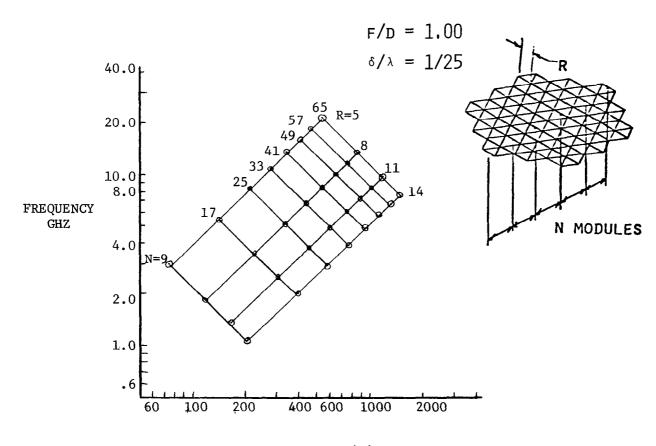






REFLECTOR DIA (M)

Figure 43. Reflector Frequency
vs
Size
(No Thermal Effects.)



REFLECTOR DIA (M)

Figure 44. Reflector Frequency vs
Size
(No Thermal Effects).

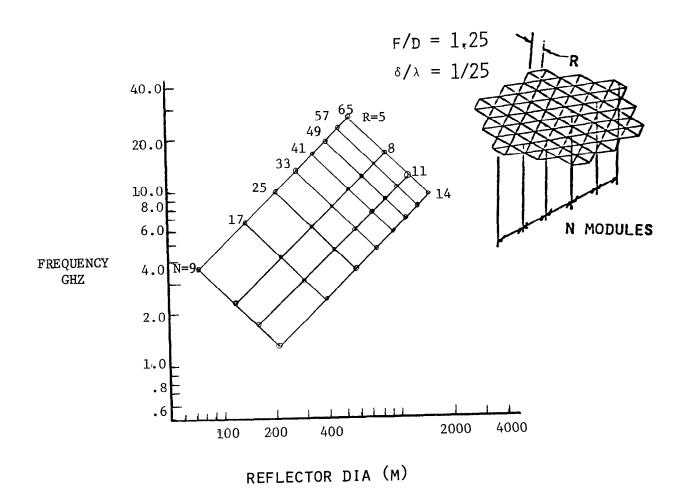


Figure 45. Reflector Frequency
vs
Size
(No Thermal Effects.)

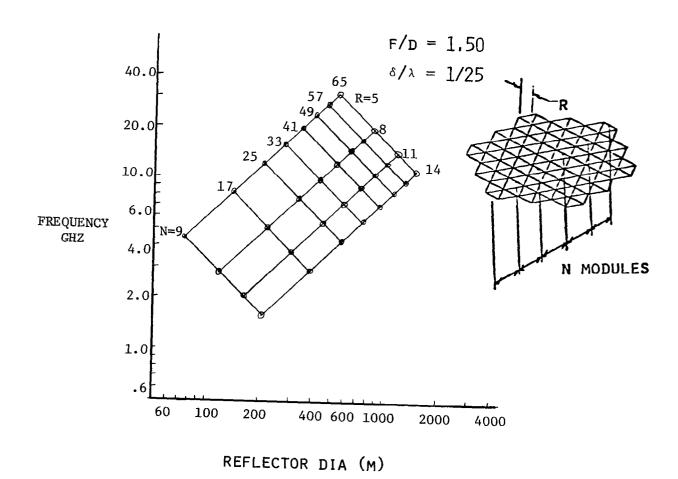


Figure 46. Reflector Frequency vs Size (No Thermal Effects).

A finite element thermal distortion model was then prepared which modeled the upper surface in order to include the distortion effects of thermal gradients in the Gr/E tubes. The thermal analysis was performed using the program "STRESS" leased to Lockheed Corporation by Tymshare Inc. The program is designed to perform linear analysis of elastically loaded structures. It can analyze structures with prismatic members or plate members, in two or three dimensions, with pinned or rigid joints, and subjected to a wide variety of loads, support motions and temperature effects. The solution technique uses finite element technique based on displacement method. The thermal condition used for this analysis assumed that the module faced the Sun directly with the upper radial arms of the mesh support surface in Sun and the lower radial arms totally shaded by the upper arms, thus creating temperature differences between arms as well as thermal gradients across the individual tubes. Figures 47 through 50 depict operation size vs frequency including the effects of thermal distortion in the support structure.

3.3 Module Assembly Techniques

Erecting large antennas in space requires construction of large numbers of modules, packaging them for launch into Earth orbit, and deploying and assembling the completed modules in the space environment. Practical means of modifying and/or repairing these structures are also required to make such systems truly economical.

3.3.1 Module to Module Attachment. Attaching elements one to another to form larger assemblies will probably provide the largest single challenge to the construction of large space structures. Certainly the assembly task of connecting modules together to form large, extremely accurate reflector poses a major design challenge and imposes significant module design requirements. The basic requirements for module to module attachment joints are listed in Table III, and Figure 51 shows the location of the joints. Figure 52

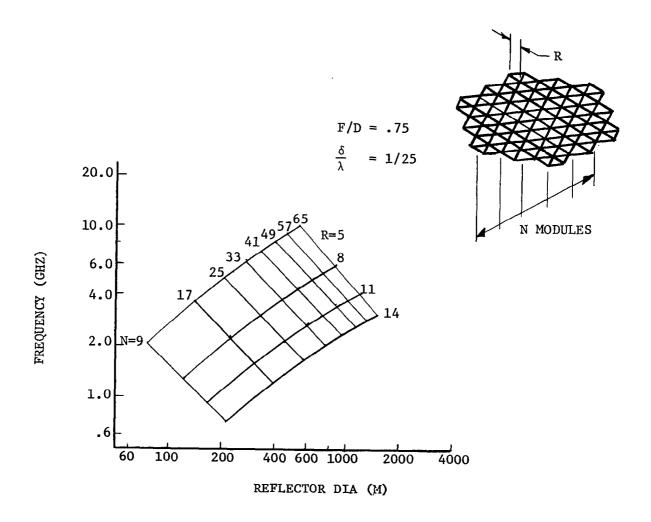


Figure 47. Reflector Frequency vs Size (Inc. Thermal Effects).

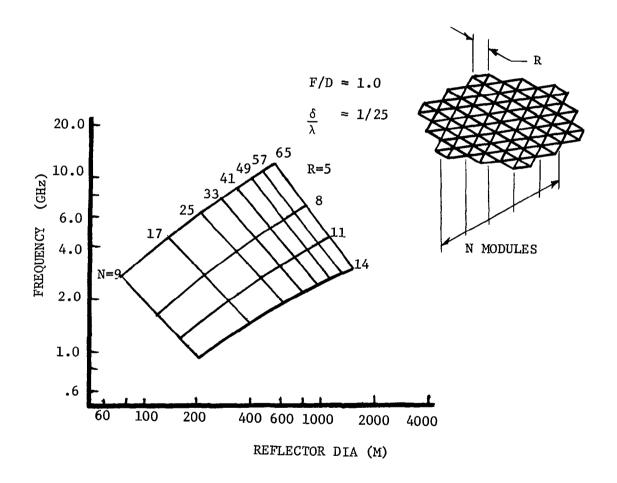


Figure 48. Reflector Frequency vs Size (Inc. Thermal Effects).

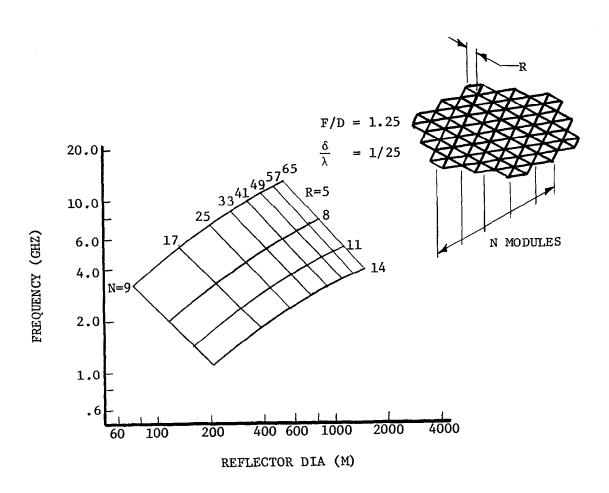


Figure 49. Reflector Frequency vs Size (Inc. Thermal Effects).

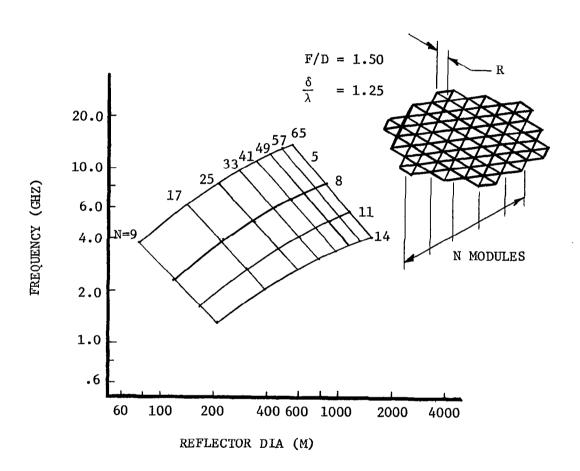


Figure 50. Reflector Frequency vs Size (Inc. Thermal Effects).

TABLE III DESIGN REQUIREMENTS FOR MODULE TO MODULE ATTACHMENT JOINTS

- Joint must have no backlash or free play.
- Joint must allow for removal/replacement of one module in an assembled reflector.
- Joint must provide positive engagement and latching.
- Joint must be capable of being made and released by a space suited astronaut.
- Joint must be compatible with the module stow/deploy motions.
- Joint should allow for one time tolerance adjustment.
- Joint should be minimum size, mass and cost.

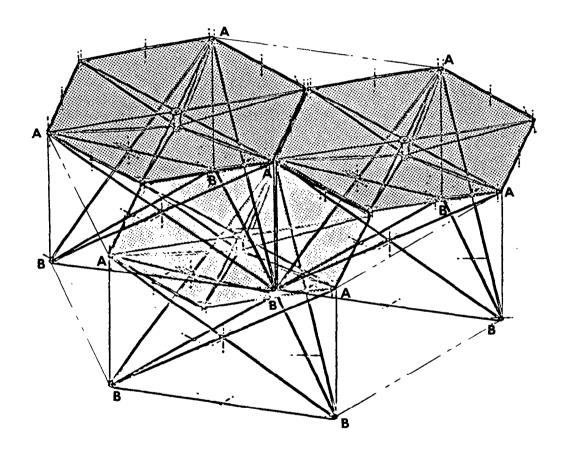


Figure 51. Module to Module Joint Locations.

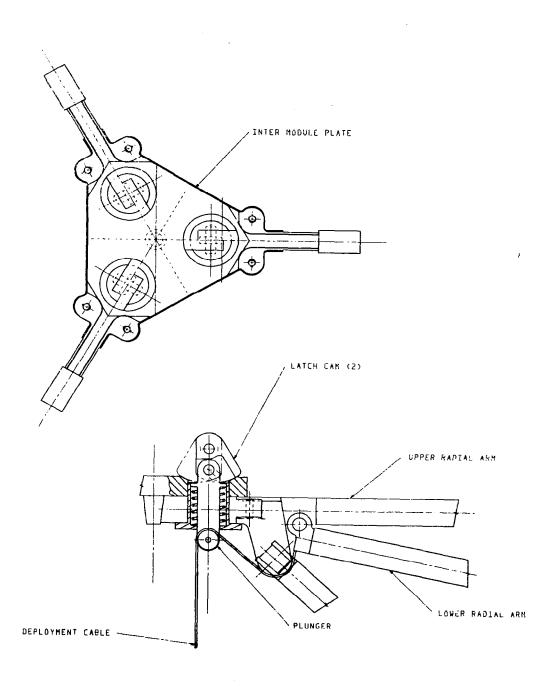


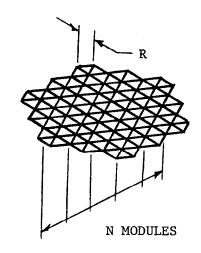
Figure 52. Module to Module Joint.

shows a design solution for the module to module attachment joints located at the corners of the reflective surface, those labeled "A" on Figure 51. The exclusive use of axial motions for activation and deactivation of the latch allows the module deployment cable to perform double service as a latch release cord. Mechanical advantages in the cam motions allow the module to be pushed into place and latched for installation. For removal, the cable is pulled, retracting the spring loaded plunger and retracking the latch cam. The wedging action of the cams against the conical seat and the edge of the module corner fitting against the center pin eliminate freeplay and provide a load path wheelbase through the joint. Other fastening devices, i.e., quarter turn fasteners, screw threads, could be used to attach each module to the cap plate, but they would require close approach by an astronaut to release the module. Using the cable release, an astronaut can perform the attachment release for both joints at each module corner from the base end of the structure, thus saving valuable EVA time and eliminating any danger associated with operating a man in close proximity to the reflective mesh.

3.3.2 Module Packaging for Launch. Packaging studies for modules in the STS Orbiter have been performed to obtain (a) the maximum size antenna reflector that can be transported in a given number of shuttle payloads, and (b) a concept for packing the stowed modules in the STS Orbiter cargo bay.

Table IV lists the number of modules necessary to complete reflectors made up of rings of modules surrounding a central module. To assemble a symmetrical reflector of increasing size, it is necessary to pack specific numbers of modules which correspond to complete rings. The table also lists the number of shuttle flights required to transport the required number of modules to orbit for assembly, assuming that they can be packaged for launch in a 25 cm diameter circle.

TABLE IV MODULE COUNT FOR INCREASING SIZE



| NUMBER OF MODULES ACROSS DIAMETER OR REFLECTOR | TOTAL MODULES IN REFLECTOR | NUMBER OF SHUTTLE FLIGHTS REQUIRED |
|---|-------------------------------|---------------------------------------|
| 1 | 1 | 1 |
| 3 | 7 | 1 |
| 5 | 19 | 1 |
| 7 | 37 | 1 |
| 9 | 61 | 1 |
| 11 | 91 | 1 |
| 13 | 127 | 1 |
| 15 | 169 | 1 |
| 17 | 217 | 1 |
| 19 | 271 | 1 |
| 21 | 331 | 1 |

TABLE IV MODULE COUNT FOR INCREASING SIZE (CONCLUDED)

| NUMBER OF MODULES ACROSS DIAMETER OR REFLECTOR | TOTAL MODULES IN REFLECTOR | NUMBER OF SHUTTLE FLIGHTS REQUIRED |
|---|----------------------------|---------------------------------------|
| 23 | 397 | 2 |
| 25 | 469 | 2 |
| 27 | 547 | 2 |
| 29 | 631 | 2 |
| 31 | 721 | 3 |
| 33 | 817 | 3 |
| 35 | 919 | 3 |
| 37 | 1027 | 4 |
| 39 | 1141 | 4 |
| 41 | 1261 | 4 |
| 43 | 1387 | 5 |
| 45 | 1519 | 5 |
| 47 | 1657 | 6 |
| 49 | 1801 | 6 |
| 51 | 1951 | 6 |
| 53 | 2167 | 7 |
| 55 | 2167 | 7 |
| 55 | 2269 | 7 |
| 57 | 2437 | 8 |
| 59 | 2611 | 8 |
| 61 | 2791 | 9 |
| 63 | 2977 | 10 |
| 65 | 3169 | 10 |

The module stowed package size is primarily dependent upon the diameter of the structural tubes and clearance allowances in the pivot joints to provide stowing space for the lower structure tubes. The tube stowing clearances are in turn dependent upon the dihedral angle of the structural cross members, which can be varied to control the overall structural depth of the module. A semi-emperical equation has been developed which relates stowed package diameter to module geometry and tubing diameter. For tube sizes and module geometries near those used in this study, the relation is:

$$D = 2 \sqrt{\left[\frac{3d}{2 \sin (30)} + \frac{(2d + .5) \sin \alpha}{\tan \theta} + 1.1 d\right]^2 + \left[2.23 d + .5\right]^2}$$

where D = package diameter - cm

d = tube diameter - cm

 α = inclination angle of cross members to mast surface plane

 $\boldsymbol{\theta}$ = true angle between cross members measured at the upper joints

for the model cross member geometry chosen:

$$D = 2\sqrt{[8.059 d + .9898]^2 + [2.23 d + .5]^2}$$

The requirements for a packaging framework to transport modules in the Orbiter cargo bay are listed in Table V. An isometric sketch of such a frame is shown in Figure 53. It consists of a number of longitudinal stringers connecting cradle sections which support the individual modules. The cradles are opened sequentially to allow the framework to dispense modules singly. Using this transport frame approach, it is possible to deploy and connect modules sequentially into reflectors of essentially unlimited aperture, by bringing more modules to the assembly site on subsequent Orbiter flights.

TABLE V MODULE PACKAGING FRAME

DESIGN REQUIREMENTS

- The frame must support all the modules through the STS launch environment.
- The frame must release modules individually for deployment, assembly.
- The frame must present no hazard to space suited astronauts when full, empty, or partially filled.
- The frame should be removable from the cargo bay while fully loaded with modules.
- The frame should be transportable in the shuttle bay when empty.



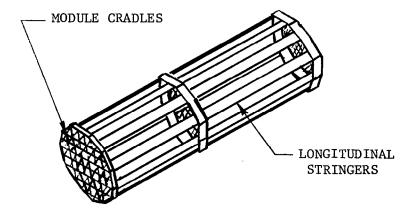
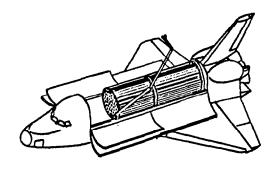


Figure 53. Module Packaging Framework.

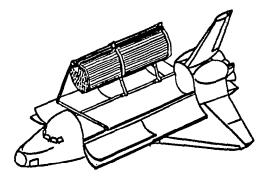
Modules are delivered to orbit in the following manner, as described in Figure 54. The loaded cannister is placed into the Orbiter cargo bay. When the Orbiter achieves the desired orbit the cargo bay doors are opened and the module cannister relocated above the cargo bay as shown in Figure 54A and B. The Payload Installation and Deployment Aide (PIDA) being developed by Johnson Space Center or an equivalent handling system can be used to affect this position change. The Orbiter RMS is then used to grasp the first module by its deployment jackscrew drive. The module cannister is designed to open sequentially and release one module at a time from its support frames. The RMS is then used to position the module away from the Orbiter and to deploy the module as shown in C. Once the module has been deployed it can be released by the RMS to be installed into a reflector assembly, D. As additional modules are deployed, the cannister structure is opened sequentially to release additional modules one at a time for deployment. The latching elements of the structure open by pivoting back against the remaining latched cannister segments to provide sufficient clearance for removal of the released module. Thus, as each row of modules is deployed, access is automatically provided to the next row of modules. After the last module is deployed, E, the cannister framework is closed and returned to the cargo bay by the PIDA, F, for return to Earth.

3.4 Reflector Assembly Scenarios

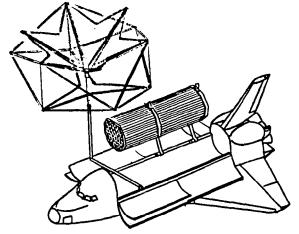
The final task required in developing large modular structures is the on orbit assembly of the total reflector from individual components. This study has identified five primary assembly procedures, and defined strengths and weaknesses among them. Primary requirements for any assembly scenario are that all required components be STS transportable, that the assembly be structurally stable throughout the construction phase, that parasitic structure be minimized, and that EVA be used only for cost effective procedures.



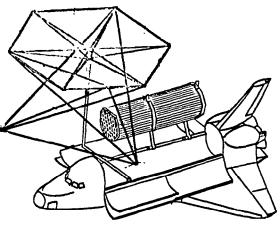
A. SHUTTLE ORBITER IN DEPLOYMENT ORBIT.



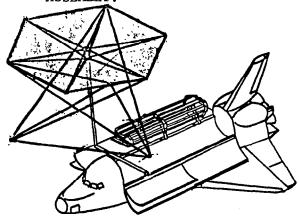
B. MODULE CANNISTER DEPLOYED BY PIDA OR EQUIVALENT PAYLOAD HANDLING MECHANISM.



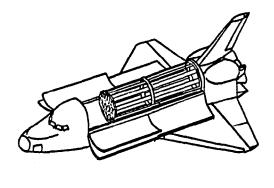
C. FIRST MODULE DEPLOYED AND READY FOR HANDOFF TO REFLECTOR ASSEMBLY.



D. FIRST MODULE REMOVED FROM CANNISTER AND BEING DEPLOYED.



E. LAST MODULE DEPLOYED AND READY FOR HANDOFF TO REFLECTOR ASSEMBLY.



F. MODULE CANNISTER RECLOSED AND REPACKED INTO ORBITER CARGO BAY FOR RETURN TO EARTH.

Figure 54. Module Deployment Scenario.

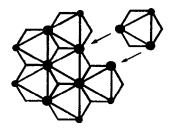
The basic assembly sequence assumed for the study is depicted in Figure 55. First, a central module is deployed, and then a ring of six modules is attached around its perimeter as shown. Additional rings of modules are simply added to the structure circumferentially around its perimeter as shown.

The simplest assembly procedure available on the space shuttle orbiter involves the use of the STS provided Remote Manipulator System (RMS) for module deployment and assembly. Figure 56 shows such an assembly. In this assembly scenario, the shuttle, equipped with two RMS arms and loaded with reflector modules is launched and achieves the desired assembly orbit. The cargo bay doors are opened and the RMS arms deployed. One arm removes the center module from the storage frame, positions it clear of the Orbiter, and deploys it. The second RMS arm then removes a second module, deploys it, and then brings the second module to the center module and either attaches the module directly or positions it in close proximity so that the final connection can be made by an astronaut. After this attachment is complete the second RMS arm removes a third module from the storage frame, deploys it, and moves it to be connected to the other two. The first RMS arm meanwhile rotates the assembly, if required, to allow access for the incoming modules. The process is continued until the reflector is complete.

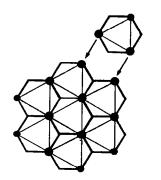
This assembly procedure is limited to reflector sizes of less than approximately 73 meters by the total reach of the RMS arms. To assemble larger reflectors the assembly would have to be "handed off" back and forth between the two RMS arms to always be able to arrange the next installation position at a point where the remaining arm could install the next module. In addition, the position placement accuracy of the RMS arms is not currently compatible with the module positioning requirements for installation without astronaut aid.



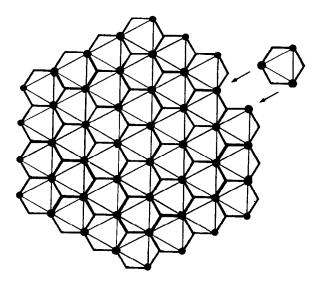
A. CENTRAL MODULE DEPLOYMENT



B. 1st PERIMETER RING INSTALLED

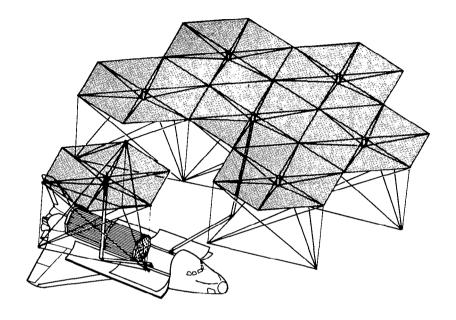


C. 2nd PERIMETER RING BEGUN



D. ADDITIONAL MODULES ADDED CIRCUMFERENTIALLY

Figure 55. Modular Reflector Assembly Order.



USE TWO RMS'S IN THE ORBITER

PHILOSOPHY

ONE RMS HOLDS AND POSITIONS THE REFLECTOR ASSEMBLY AND THE SECOND RMS DEPLOYS AND INSTALLS ADDITIONAL MODULES

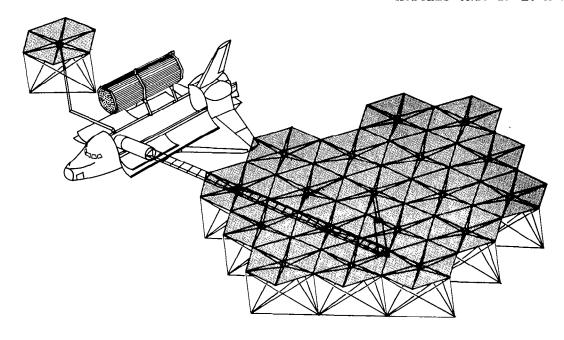
Figure 56. Modular Antenna Assembly Scenario.

The second assembly procedure investigated is depicted in Figure 57. In this concept an extendable assembly boom is used to hold the reflector assembly, the standard RMS arm is used to remove modules from the storage cannister and deploy them, and astronauts equipped with Manned Maneuvering Units (MMU) transfer the deployed modules from the RMS arm to the reflector. In sequence, the Orbiter achieves orbit, opens the cargo bay and deploys the RMS arm, the reflector assembly boom and module cannister. As each module is deployed, it is removed from the RMS arm by an MMU equipped astronaut, who transports the module to its proper assembly position in the reflector. The module is then installed by two astronauts, one operating the front reflective surface attachments and one connecting the rear surface attachments. As each module is being installed, a third astronaut controlling the RMS arm from within the Orbiter removes the next module from the storage cannister and deploys it, preparing it for pickup and transfer to the reflector assembly. When the reflector is complete, the assembly boom can either be removed from the reflector, retracted and returned to Earth with the Shuttle, or left with the reflector as part of the feed support tower.

This assembly scenario is essentially limited to the maximum diameter reflector transportable in one shuttle flight (approximately 310 m) unless docking provisions with the assembly boom are provided. While the shuttle cargo bay can hold enough modules, 330, to construct a reflector approximately 475 m across the corners, if volume is allocated for an assembly fixture and/or feed mast, the maximum practical reflector diameter for a single launch drops to approximately 310 meters. The transfer of modules from the RMS to the assembly requires extensive EVA by Astronauts.

The third assembly scenario attempts to ease the astronaut's work level by articulating the assembly boom. This approach, shown in Figure 58, differs significantly from the previous scenario only in the construction of the assembly boom. In this case, the reflector assembly can be rotated and tilted at its attachment point on the boom, and the

USE RMS AND ASTRONAUT TO INSTALL MODULES ONTO DEPLOYABLE BOOM



PHILOSOPHY

AN ASSEMBLY BOOM IS DEPLOYED FROM THE ORBITER. THE RMS HOLDS EACH MODULE FOR DEPLOYMENT, AFTER WHICH ASTRONAUTS TRANSPORT IT TO THE ASSEMBLY USING MMU

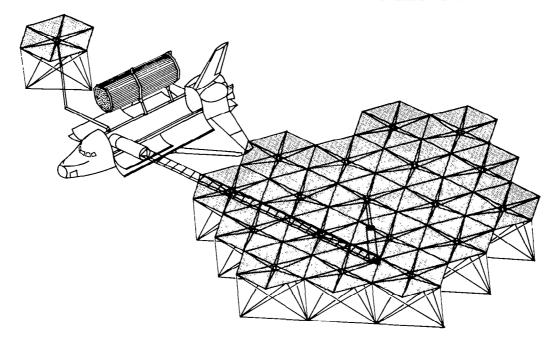
boom can be extended and retracted during the assembly process. The actual construction process is identical to that of scenario 2, but since the partially completed reflector can be rotated and tilted to position the next sequential module attach point next to the Orbiter cargo bay, astronaut travel time transporting modules is minimized. In fact, using the RMS and articulated boom, an operator located within the shuttle can position each module within a meter of its final installation position. The astronaut them performs the final alignment and makes the connector attachments. This assembly method suffers the same reflector size limitations (approximately 310 m) as scenario 2, but the astronaut EVA work is considerably reduced, and possibly eliminated if the RMS arm positioning accuracy can be improved.

To produce large reflector apertures (> 300 m in diameter) assembly methods which use multiple shuttle flights to supply parts for a single reflector must be employed.

Assembly scenario 4 (shown in Figure 59) uses a free flying satellite as an assembly platform for the reflector. The assembly satellite consists of a multi-mission satellite body with an articulated reflector support attached to the top, the support for the extendable boom which in turn supports the solar arrays and a module installation arm. The initial shuttle flight deploys the satellite and delivers what modules can be carried in the remaining cargo bay volume. The Orbiter achieves a synchronized close formation to the satellite and deploys the cannister package. The modules are removed from the cannister and deployed by the RMS. They are then transferred to the installation arm of the satellite for attachment to the reflector.

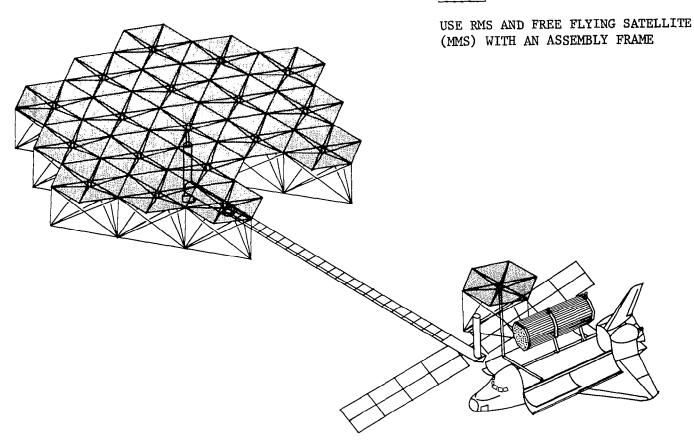
The articulated arm rotates and tilts the reflector to align the next module installation position with the extendable arm. This arm is retracted until the new module is correctly positioned, and the module is then attached by extending the module support arm. After the module

USE RMS AND AN ARTICULATED ASSEMBLY BOOM



PHILOSOPHY

THE RMS REMOVES EACH MODULE, DEPLOYS IT, AND ATTACHES IT TO THE ASSEMBLY. THE ARTICULATED BOOM POSITIONS THE REFLECTOR TO RECEIVE EACH NEW MODULE



PHILOSOPHY

THE RMS DEPLOYS EACH MODULE AND TRANSFERS IT TO THE ASSEMBLY SATELLITE WHICH THEN INSTALLS IT INTO THE REFLECTOR

is attached the module support arm is retracted to clear the module backup structure, and the arm is extended to receive another module from the Shuttle. When the reflector is complete, a feed assembly can be attached to the module support beam which then extends to become the vertical portion of the feed support tower.

The primary difficulty in this assembly is the interactive control of two independent spacecraft during the time when the module is being held by both the shuttle RMS arm and the satellite module support boom. The problems involved when two independently controlled spacecraft are in contact have been documented since the Gemini Program. An alternative solution to the transfer problem would be for an MMU equipped astronaut to transfer the modules either to the support boom, or to install them directly onto the reflector assembly, using the satellite's extendable boom solely as a support for the feed tower.

Rather than transferring modules from the Shuttle Orbiter to the assembly satellite one by one, the entire cannister of modules could be moved to the satellite, and deployed and installed by a manipulator arm on the satellite, as shown in Figure 60. The Shuttle Orbiter then would be used as a transport vehicle and control station for the servo-mechanisms aboard the assembly satellite which would remove the modules from the storage cannister, deploy them, and install them. Again in this scenario, MMV equipped astronauts could remove the deployed modules from the manipulator arm, position them, and attach them to the assembly. The size of these reflectors is limited only by the number of STS launches that can be dedicated to their construction. Table VI summarizes the assembly techniques discussed in this section along with their advantages, disadvantages, and areas of technological development required for their fulfillment.

USE SHUTTLE ORBITER AND AN AUTOMATED FREE FLYING SATELLITE (MMS) WITH AN ASSEMBLY FRAME

PHILOSOPHY

THE SHUTTLE ORBITER DELIVERS CANNISTERS OF MODULES TO THE ASSEMBLY SATELLITE. THE SATELLITE IS EQUIPPED WITH A MANIPULATOR ARM AND SERVO-MECHANISMS TO REMOVE MODULES FROM THE CANNISTER, DEPLOY THEM, AND INSERT THEM INTO THE REFLECTOR ASSEMBLY

TABLE VI REFLECTOR ASSEMBLY TECHNIQUES

| METHOD | advantages | DISADVANTAGES | NEW TECHNOLOGY REQUIRED |
|---|--|--|---|
| 1. Assembly By 2 RMS's | o Least technology required | o Limited to = 73 Meters by reach of RMS arms O Potential damage to modules by Orbiter attitude control | o Method for offset module contour determination o Development of storage cannister |
| 2. Assembly Using Astronaut, RMS, and Boom | o Allows larger size reflectors than method l without added complexity of active assembly frames | o Potential damage to modules by Orbiter attitude control o Possible Orbiter attitude control effects due to variation in moment of inertia o Size limited to one shuttle launch capability (= 310 Meters Diameter) o Man required to free fly | o Method for offset module contour determination o Development of storage cannister o Safety aspects of free flying astronaut o Development of boom |
| 3. Assembly By RMS and Articulated Boom Pixture | o EVA not required | o Potential damage to modules by Orbiter attitude control o Possible Orbiter attitude control effects due to variation of moment of inertia o Size limited to one shuttle launch capability (= 310 Neters Diameter) | o Method for offset module contour determination o Development of storage cannister o Development of Boom o Development of boom articulation servos |
| 4. Assembly by Free Flying Satellite | o No site limit o Self contained power and attitude control | O Control fuel for flying formation for extended periods Transfer of module between two independent spacecraft Automated assembly servo systems required | o Method for offset module contour determination o Development of storage cannister o Development of boom o Development of boom articulation servos o Method of slaving attitude control of one spacecraft to another |
| 5. Assembly by Free Flying Automated Satellite | o No size limit o Self contained power and attitude control o No dual spacecraft control problems | o Control of automation sequence of deployment and insertion of modules | o Method for offset module contour determination o Development of storage container o Development of boom o Development of boom articulation servos o Development of automation sequencing, controi |

4.0 CONCLUSIONS

4.1 Modular Antenna Feasibility

The kinematic studies and Engineering Demonstration Model developed during this study have fully verified the deployment kinematics, stowing philosophy, and deployment sequencing for large deployable antenna modules. These studies have established that such modules can be stowed in packages as small as 25 cm in diameter, using 1.27 cm diameter structural tubes. Mesh attachment methods compatible with full scale modules have been devised. Parametric studies of large modular reflectors using 1.27 cm diameter struts as structural elements have established size, mass and aperture frequency capabilities for these assemblies. Specific mission requirements should however be reviewed to verify tube sizing for each application. Preliminary studies have been made devising means of delivering modules to orbit, and once there, of assembling the modules into complete modular antenna reflectors. The basic feasibility of creating mass efficient modules, erectable into large structures in space has been established.

4.2 Recommendations for Further Study

The current study has established the feasibility of constructing modular elements for assembly into large structures. The module configuration used for this study maximize both the individual module diameter and backup structure depth in its stowed package. However, the kinematic requirement for folding the cross braces does complicate control of the module deployment and force the use of a fairly complex joint at the cross brace fold joint. For applications in which the depth of the backup structure can be reduced, simpler kinematic models can be constructed which use single piece cross braces.

Two candidate configurations for further study are shown in Figures 61 and 62. The first configuration uses cross braces which are pivoted at the mid-point. Therefore, when stowed, the cross braces scissors closed forcing the bottom struts to fold, allowing the deployment motion to be controlled entirely by the central jackscrew. The size limiting element for this configuration would be the length of the cross brace. Assuming a minimum structural depth of one half the module diameter, the cross brace length would be equal to the module diameter. Thus the maximum module size packageable in the Shuttle Orbiter is approximately 14 m. Several modules could possibly be ganged together, however, to deploy as a single unit.

The module shown in Figure 62 rearranges the cross braces into a drum shaped configuration. These cross arms fold inward parallel to the stowed package centerline as the radial arms stow, forcing the lower arms to fold. This configuration also eliminates the kinematic need for the deployment cable. The lower ends of the cross braces can be released sequentially for deployment. As in the previous configuration, the length of the cross braces can be varied to provide desired structural depth. Again assuming that a reasonable minimum structure of depth is one half the diameter, the cross brace elements would be approximately 1.32 times the module radius, thus limiting the modules transported in the Orbiter to approximately 21 meters in diameter. If even less structural depth were required these modules could approach 28 m diameter as a limit for zero structural depth. The precise kinematics of these module styles should be investigated to provide a full family of module configurations which would be compatible with a wide variety of potential antenna reflector applications.

The second area of investigation which should be pursued is refinement of the process of assembling many modular elements into single structures. This study would involve full detail design of module to module joints and fabrication of seven modules, which would allow operational

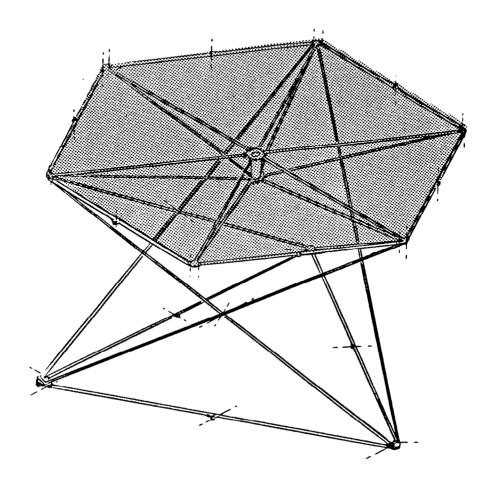


Figure 61. Alternate Module Configuration (Pivoted Cross Braces).

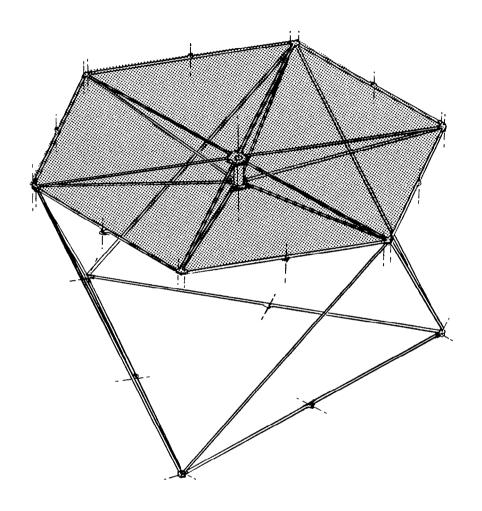


Figure 62. Alternate Module Configuration (Drum Style Cross Braces).

testing of both the module to module joining process and the replacement of one module either at the edge of or in the center of a reflector assembly. By assemblying seven modules, one center module and six surrounding modules, the general problem of structural assembly in either 1g or at neutral bouyancy can be evaluated, and realistic estimates of required assembly time can be obtained. Successful completion of the process would demonstrate the feasibility of structural assembly without support stands.

A third area of extended research would investigate increasing the effective size and/or operational frequency limit of each deployable module. The module size limits can be extended by developing the kinematics associated with deploying several modules simultaneously. This approach would allow deployment of sets of up to seven modules at once, thus decreasing the number of deployed modular elements required to construct a given reflector by a factor of seven, and reducing the orbital assembly time accordingly. The operational frequency can be increased by reducing the effective RMS surface error. Two approaches to this problem are to use a thin, flexible membrane with double curvature in place of the mesh surface, or to install separate rigid surface panels onto the erected modular subsurface. Such techniques, if successful, could extend the operational frequency into the millimeter wavelength range.

| | | 1 |
|--|--|-----|
| | | - 1 |

APPENDIX A

MODULAR ANTENNA PERFORMANCE STUDIES

5 28.000 METERS -0.75 88.61052 METERS 116.62178 METERS 118.14736 METERS 26.3193736 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

9 28.000 METERS 0.75 157.37147 METERS 207.11920 METERS 209.82862 METERS 14.8052589 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

13 28.000 METERS 0.75 226.13242 METERS 297.61663 METERS 301.50989 METERS 10.3009963 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

17 28.000 METERS 0.75 294.89336 METERS 388.11405 METERS 393.19115 METERS 7.8983905 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

21 28.000 METERS 0.75 363.65431 METERS 478.61147 METERS 484.87241 METERS 6.4046608 MM

25 28.000 METERS 0.75 432.41526 METERS 569.10889 METERS 576.55367 METERS 5.3860871 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

29 28.000 METERS 0.75 501.17620 METERS 659.60632 METERS 668.23493 METERS 4.6470513 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

33 28.000 METERS 0.75 569.93714 METERS 750.10374 METERS 759.91619 METERS 4.0863606 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

37 28.000 METERS 0.75 638.69810 METERS 840.60117 METERS 851.59746 METERS 3.6464064 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

41 28.000 METERS 0.75 707.45904 METERS 931.09859 METERS 943.27872 METERS 3.2919806 MM NO OF MODULES ACROSS CORNERS= 45

MODULE DIAMETER ACROSS CORNERS= 28.000 METERS

FOCAL LENGTH TO DIAMETER RATIO= 0.75

FOCAL LENGTH OF REFLECTOR= 776.21999 METERS

REFLECTOR PHYSICAL DIAMETER= 1021.59602 METERS

REFLECTOR ELECTRICAL DIAMETER= 1034.95999 METERS

SURFACE APPROXIMATION ERROR= 3.0003515 MM

NO OF MODULES ACROSS CORNERS= 49

MODULE DIAMETER ACROSS CORNERS= 28.000 METERS

FOCAL LENGTH TO DIAMETER RATIO= 0.75

FOCAL LENGTH OF REFLECTOR= 844.98093 METERS

REFLECTOR PHYSICAL DIAMETER= 1112.09343 METERS

REFLECTOR ELECTRICAL DIAMETER= 1126.64124 METERS

SURFACE APPROXIMATION ERROR= 2.7561880 MM

NO OF MODULES ACROSS CORNERS= 53

MODULE DIAMETER ACROSS CORNERS= 28.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 0.75

FOCAL LENGTH OF REFLECTOR= 913.74187 METERS
REFLECTOR PHYSICAL DIAMETER= 1202.59085 METERS
REFLECTOR ELECTRICAL DIAMETER= 1218.32249 METERS
SURFACE APPROXIMATION ERROR= 2.5487736 MM

NO OF MODULES ACROSS CORNERS= 57

MODULE DIAMETER ACROSS CORNERS= 28.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 0.75

FOCAL LENGTH OF REFLECTOR= 982.50282 METERS
REFLECTOR PHYSICAL DIAMETER= 1293.08827 METERS
REFLECTOR ELECTRICAL DIAMETER= 1310.00375 METERS
SURFACE APPROXIMATION ERROR= 2.3703923 MM

NO OF MODULES ACROSS CORNERS= 61
MODULE DIAMETER ACROSS CORNERS= 28.000 METERS
FOCAL LENGTH TO DIAMETER RATID= 0.75
FOCAL LENGTH OF REFLECTOR= 1051.26376 METERS
REFLECTOR PHYSICAL DIAMETER= 1383.58569 METERS
REFLECTOR ELECTRICAL DIAMETER= 1401.68501 METERS
SURFACE APPROXIMATION ERROR= 2.2153468 MM

NO OF MODULES ACROSS CORNERS= 65 MODULE DIAMETER ACROSS CORNERS= 28.000 METERS FOCAL LENGTH TO DIAMETER RATIO= 8.75 FOCAL LENGTH OF REFLECTOR= 1120.02473 METERS REFLECTOR PHYSICAL DIAMETER= 1474.08313 METERS REFLECTOR ELECTRICAL DIAMETER= 1493.36630 METERS 2.0793390 MM SURFACE APPROXIMATION ERROR=

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

22.000 METERS 0.7569.62255 METERS 91.63140 METERS 92.83007 METERS 20.6795080 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 164.86535 METERS SURFACE APPROXIMATION ERROR=

22.000 METERS 0.75123.64901 METERS 162.73652 METERS 11.6327033 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 236.90063 METERS SURFACE APPROXIMATION ERROR=

13 22.000 METERS 0.75177.67547 METERS 233.84163 METERS 8.0936400 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 308.93590 METERS SURFACE APPROXIMATION ERROR=

17 22.000 METERS 0.75231.70193 METERS 304.94675 METERS 6.2058782 MM

21 22.000 METERS 0.75 285.72838 METERS 376.05187 METERS 380.97118 METERS 5.0322335 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

25 22.000 METERS 0.75 339.75484 METERS 447.15699 METERS 453.00645 METERS 4.2319256 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

29 22.000 METERS 0.75 393.78130 METERS 518.26211 METERS 525.04173 METERS 3.6512547 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

33 22.000 METERS 0.75 447.80776 METERS 589.36723 METERS 597.07701 METERS 3.2107119 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SUPFACE APPROXIMATION EPPOR=

37 22.000 METERS 0.75 501.83422 METERS 660.47234 METERS 669.11229 METERS 2.8650336 MM

41 22.000 METERS 0.75555.86068 METERS 731.57746 METERS 2.5865561 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 813.18285 METERS SURFACE APPROXIMATION ERROR=

45 22.000 METERS 0.75609.88714 METERS 802.68258 METERS 2.3574191 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 885.21811 METERS SURFACE APPROXIMATION ERROR=

49 22.000 METERS 0.75663.91358 METERS 873.78769 METERS 2.1655763 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 957.25339 METERS SURFACE APPROXIMATION ERROR= -

53 22.000 METERS 0.75717.94004 METERS 944.89281 METERS 2.0026079 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 1029.28867 METERS SURFACE APPROXIMATION ERROR=

57 22.000 METERS 0.75 771.96650 METERS 1015.99793 METERS 1.8624511 MM

17 16.000 METERS 0.75168.51049 METERS 221.77946 METERS 4.5133660 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 277.06995 METERS SURFACE APPROXIMATION FRACE -

21 16.000 METERS 0.75207.80246 METERS 273.49227 METERS 3.6598062 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

25 16.000 METERS 0.75247.09443 METERS 325.20508 METERS 329.45924 METERS 3.0777640 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 381.84853 METERS SURFACE APPROXIMATION ERROR=

29 16.000 METERS 0.75286.38640 METERS 376.91790 METERS 2.6554579 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 434.23782 METERS SURFACE APPROXIMATION ERROR=

33 16.000 METERS 0.75325.67837 METERS 428.63071 METERS 2.3350632 MM

NO OF MODULES ACROSS CORNERS= 61 MODULE DIAMETER ACROSS CORNERS= 22.000 METERS FOCAL LENGTH TO DIAMETER RATIO= 0.75 FOCAL LENGTH OF REFLECTOR= 825.99296 METERS REFLECTOR PHYSICAL DIAMETER= 1087.10304 METERS REFLECTOR ELECTRICAL DIAMETER= 1101.32394 METERS SURFACE APPROXIMATION ERROR= 1.7406296 MM

NO OF MODULES ACROSS CORNERS= 65 MODULE DIAMETER ACROSS CORNERS= 22.000 METERS FOCAL LENGTH TO DIAMETER RATIO= 0.75FOCAL LENGTH OF REFLECTOR= 880.01943 METERS REFLECTOR PHYSICAL DIAMETER= 1158.20818 METERS REFLECTOR ELECTRICAL DIAMETER= 1173.35924 METERS SURFACE APPROXIMATION ERROR= 1.6337664 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

5 16.000 METERS 0.75 50.63458 METERS 66.64102 METERS 67.51278 METERS 15.0396421 MM

NO DE MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

16.000 METERS 0.7589.92655 METERS 118.35383 METERS 119.90207 METERS 8.4601479 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 172.29136 METERS SURFACE APPROXIMATION ERROR=

13 16.000 METERS 0.75129.21852 METERS 170.06664 METERS 5.8862836 MM

37 16.000 METERS 0.75364.97034 METERS 480.34352 METERS 2.0836608 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 539.01641 METERS SURFACE APPROXIMATION ERROR=

41 16.000 METERS 0.75404.26231 METERS 532.05634 METERS 1.8811317 MM

NO DE MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

45 16.000 METERS 0.75443.55428 METERS 583.76915 METERS 591.40571 METERS 1.7144866 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 643.79499 METERS SURFACE APPROXIMATION ERROR=

49 16.000 METERS 0.75482.84624 METERS 635.48196 METERS 1.5749646 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 696.18429 METERS SURFACE APPROXIMATION ERROR=

53 16.000 METERS 0.75522.13821 METERS 687.19477 METERS 1.4564421 MM

57 16.000 METERS 0.75 561.43018 METERS 738.90759 METERS 748.57358 METERS 1.3545099 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

61 16.000 METERS 0.75 600.72216 METERS 790.62040 METERS 800.96288 METERS 1.2659124 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

65 16.000 METERS 0.75 640.01412 METERS 842.33321 METERS 853.35217 METERS 1.1881937 MM

MO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

5 10.000 METERS 0.75 31.64662 METERS 41.65064 METERS 42.19549 METERS 9.3997763 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

9 10.000 METERS 0.75 56.20410 METERS 73.97114 METERS 74.93879 METERS 5.2875924 MM

13 10.000 METERS 0.75 80.76158 METERS 106.29165 METERS 107.68210 METERS 3.6789273 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

17 10.000 METERS 0.75 105.31906 METERS 138.61216 METERS 140.42541 METERS 2.8208538 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

21 10.000 METERS 0.75 129.87654 METERS 170.93267 METERS 173.16872 METERS 2.2873789 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

25 10.000 METERS 0.75 154.43402 METERS 203.25318 METERS 205.91203 METERS 1.9236025 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

29 10.000 METERS 0.75 178.99150 METERS 235.57368 METERS 238.65533 METERS 1.6596612 MM

33 10.000 METERS 0.75 203.54898 METERS 267.89419 METERS 1.4594145 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

37 10.000 METERS 0.75228.10646 METERS 300.21470 METERS 304.14195 METERS 1.3022880 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= 1 EDCAL LENGTH DE REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= -SURFACE APPROXIMATION ERROR=

41 10.000 METERS 0.75252,66394 METERS 332.53521 METERS 336.88526 METERS 1.1757073 MM

NO DE MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

45 10.000 METERS 0.75277.22142 METERS 364.85572 METERS 369.62857 METERS 1.0715541 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 402.37187 METERS SURFACE APPROXIMATION ERROR=

49 10.000 METERS 0.75301.77890 METERS 397.17622 METERS 0.9843529 MM

53 10.000 METERS 9.75 326.33638 METERS 429.49673 METERS 435.11518 METERS 0.9102763 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

57 10.000 METERS 0.75 350.89386 METERS 461.81724 METERS 467.85849 METERS 0.8465687 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

61 10.000 METERS 0.75 375.45135 METERS 494.13775 METERS 500.60180 METERS 0.7911953 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

65 10.000 METERS 0.75 400.00883 METERS 526.45826 METERS 533.34511 METERS 0.7426211 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER

5 28.000 METERS 1.00 117.50216 METERS

1.00 117.50216 METERS 116.62178 METERS 19.9793613 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 208.68274 METERS SURFACE APPROXIMATION ERROR=

9 28.000 METERS 1.00 208.68274 METERS 207.11920 METERS 11.2438538 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 299.86333 METERS SURFACE APPROXIMATION ERROR=

13 29.000 METERS 1.00 299.86333 METERS 297.61663 METERS 7.8239220 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 391.04392 METERS SURFACE APPROXIMATION ERROR=

17 29.000 METERS 1.00391.04392 METERS 388.11405 METERS 5.9993143 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 482.23451 METERS SURFACE APPROXIMATION ERROR=

21 28.000 METERS 1.00 492.22**4**51 METERS 478.61147 METERS 4.8648313 MM

25 29.000 METERS 1.00 573.40510 METERS 569.10999 METERS 4.0911920 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SUBSECT APPROXIMATION FRADE-

29 29.000 METERS 1.00 664.58569 METERS 659.60632 METERS 664.58569 METERS 3.5298556 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

33 29.000 METERS 1.00 755.76627 METERS 750.10374 METERS 755.76627 METERS 3.1039743 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

37 29.000 METERS 1.00 846.94687 METERS 940.60117 METERS 846.94687 METERS 2.7697965 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 938.12746 METERS SURFACE APPROXIMATION ERROR=

41 28.000 METERS 1.00 938.12746 METERS 931.09859 METERS 2.5005816 MM

NO OF MODULES ACROSS CORNERS= 45
MODULE DIAMETER ACROSS CORNERS= 28.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 1.00
FOCAL LENGTH OF REFLECTOR= 1029.30804 METERS
REFLECTOR PHYSICAL DIAMETER= 1021.59602 METERS
REFLECTOR ELECTRICAL DIAMETER= 1029.30804 METERS
SURFACE APPROXIMATION ERROR= 2.2790647 MM

NO OF MODULES ACROSS CORNERS= 49

MODULE DIAMETER ACROSS CORNERS= 28.000 METERS
FOCAL LENGTH OF REFLECTOR= 1.00

FOCAL LENGTH OF REFLECTOR= 1120.48863 METERS
REFLECTOR PHYSICAL DIAMETER= 1120.48863 METERS
REFLECTOR ELECTRICAL DIAMETER= 1120.48863 METERS
SURFACE APPROXIMATION ERROR= 2.0936010 MM

NO OF MODULES ACROSS CORNERS= 53
MODULE DIAMETER ACROSS CORNERS= 28.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 1.00
FOCAL LENGTH OF REFLECTOR= 1211.66922 METERS
REFLECTOR PHYSICAL DIAMETER= 1202.59085 METERS
REFLECTOR ELECTRICAL DIAMETER= 1211.66922 METERS
SURFACE APPROXIMATION ERROR= 1.9360509 MM

NO OF MODULES ACROSS CORNERS= 57

MODULE DIAMETER ACROSS CORNERS= 28.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 1.00

FOCAL LENGTH OF REFLECTOR= 1302.84981 METERS
REFLECTOR PHYSICAL DIAMETER= 1293.08827 METERS
REFLECTOR ELECTRICAL DIAMETER= 1302.84981 METERS
SURFACE APPROXIMATION ERROR= 1.8005538 MM

NO OF MODULES ACROSS CORNERS= 61

MODULE DIAMETER ACROSS CORNERS= 28.000 METERS

FOCAL LENGTH TO DIAMETER RATIO= 1.00

FOCAL LENGTH OF REFLECTOR= 1394.03040 METERS

REFLECTOR PHYSICAL DIAMETER= 1394.03040 METERS

REFLECTOR ELECTRICAL DIAMETER= 1394.03040 METERS

SURFACE APPROXIMATION ERROR= 1.6827821 MM

NO OF MODULES ACPOSS CORNERS= 65

MODULE DIAMETER ACPOSS CORNERS= 28.000 METERS

FOCAL LENGTH TO DIAMETER RATIO= 1.00

FOCAL LENGTH OF REFLECTOR= 1485.21100 METERS

REFLECTOR PHYSICAL DIAMETER= 1474.08313 METERS

REFLECTOR ELECTRICAL DIAMETER= 1485.21100 METERS

SURFACE APPROXIMATION ERROR= 1.5794711 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

5 22.000 METERS 1.00 92.32312 METERS 91.63140 METERS 92.32312 METERS 15.6980695 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

9 22.000 METERS 1.00 163.96501 METERS 162.73652 METERS 163.96501 METERS 8.8344567 MM

NO DE MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

13 22.000 METERS 1.00 235.60691 METERS 233.84163 METERS 235.60691 METERS 6.1473673 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

17 22.000 METERS 1.00 307.24879 METERS 304.94675 METERS 307.24879 METERS 4.7137470 MM

21 22.000 METERS 1.00 378.89069 METERS 376.05187 METERS 3.8223675 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 450.53258 METERS SURFACE APPROXIMATION ERROR=

25 22.000 METERS 1.00 450.53258 METERS 447.15699 METERS 3.2145080 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

29 22.000 METERS 1.00522.17447 METERS 518.26211 METERS 522.17447 METERS 2.7734580 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 593,81636 METERS SURFACE APPROXIMATION ERROR=

33 22.000 METERS 1.00 593.81636 METERS 589.36723 METERS 2.4388370 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 665.45825 METERS SURFACE APPROXIMATION ERROR=

37 22.000 METERS 1.00 665.45825 METERS 660.47234 METERS 2.1762687 MM

41 22.000 METERS 1.00 737.10014 METERS 731.57746 METERS 1.9647427 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

45 22.000 METERS 1.00 808.74203 METERS 802.68258 METERS 808.74203 METERS 1.7906937 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

49 22.000 METERS 1.00 880.38392 METERS 873.78769 METERS 880.38392 METERS 1.6449722 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

53 22.000 METERS .1.00 952.02581 METERS 944.89281 METERS 952.02581 METERS 1.5211829 MM

NO OF MODULES ACROSS CORNERS= 57 MODULE DIAMETER ACROSS CORNERS= 22.000 METERS FOCAL LENGTH TO DIAMETER RATIO= 1.00 FOCAL LENGTH OF REFLECTOR= 1023.66771 METERS REFLECTOR PHYSICAL DIAMETER= -1015.99793 METERS REFLECTOR ELECTRICAL DIAMETER= 1023.66771 METERS SURFACE APPROXIMATION ERROR= 1.4147208 MM

NO OF MODULES ACROSS CORNERS= 61
MODULE DIAMETER ACROSS CORNERS= 22.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 1.00
FOCAL LENGTH OF REFLECTOR= 1095.30959 METERS
REFLECTOR PHYSICAL DIAMETER= 1087.10304 METERS
REFLECTOR ELECTRICAL DIAMETER= 1095.30959 METERS
SURFACE APPROXIMATION ERROR= 1.3221859 MM

NO OF MODULES ACROSS CORNERS= 65
MODULE DIAMETER ACROSS CORNERS= 22.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 1.00
FOCAL LENGTH OF REFLECTOR= 1166.95149 METERS
REFLECTOR PHYSICAL DIAMETER= 1158.20818 METERS
REFLECTOR ELECTRICAL DIAMETER= 1166.95149 METERS
SURFACE APPROXIMATION ERROR= 1.2410130 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

5 16.000 METERS 1.00 67.14409 METERS 66.64102 METERS 67.14409 METERS 11.4167779 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

9 16.000 METERS 1.00 119.24728 METERS 118.35383 METERS 119.24728 METERS 6.4250593 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

13 16.000 METERS 1.00 171.35048 METERS 170.06664 METERS 171.35048 METERS 4.4709126 MM

17 16.000 METERS 1.00 223.45367 METERS 221.77946 METERS 3.4281796 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 275.55686 METERS SURFACE APPROXIMATION ERROR=

21 16.000 METERS 1.00 275.55686 METERS 273.49227 METERS 2.7799036 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR= |

25 16.000 METERS 1.00 327.66006 METERS 325.20508 METERS 327.66006 METERS 2.3378240 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 379.76325 METERS SURFACE APPROXIMATION ERROR=

29 16.000 METERS 1.00 379.76325 METERS 376.91790 METERS 2.0170603 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 431.86644 METERS SURFACE APPROXIMATION ERROR=

33 16.000 METERS 1.00 431.86644 METERS 428.63071 METERS 1.7736996 MM

27 1.00 483.96964 METERS 480.34352 METERS 483.96964 METERS 1.5827409 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR FLECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

41 16.000 METERS 1.00 536.07283 METERS 532.05634 METERS 536.07283 METERS 1.4289038 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION FRACE=

45 16.000 METERS 1.00588.17603 METERS 583.76915 METERS 588.17603 METERS 1.3023227 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

49 16.000 METERS -1.00 640.2**79**21 METERS 635.48196 METERS 640.27921 METERS 1.1963434 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= | REFLECTOR ELECTRICAL DIAMETER= 692.38241 METERS SURFACE APPROXIMATION FRACE=

50 16.000 METERS 1.00 692.38241 METERS 687.19477 METERS 1.1063148 MM

57 16.000 METERS 1.00 744.48560 METERS 738.90759 METERS 1.0288879 MM

NO DE MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER=, 796.58880 METERS SURFACE APPROXIMATION ERROR=

61 16.000 METERS 1.00 796.58880 METERS 790.62040 METERS 0.9615898 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR= |

65 16.000 METERS 1.00 848.69199 METERS 842.33321 METERS 848.69199 METERS 0.9025549 MM

MO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

10.000 METERS 1.00 41.96506 METERS 41.65064 METERS 41.96506 METERS 7.1354862 MM

NO DE MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

10.000 METERS 1.00 74.52955 METERS 73.97114 METERS 74.52955 METERS 4.0156621 MM

13 10.000 METERS 1.00 107.09405 METERS 106.29165 METERS 2.7942578 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

17 10.000 METERS 1.00 139.65854 METERS 138.61216 METERS 139.65854 METERS 2.1426122 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

21 10.000 METERS 1.00 172.22304 METERS 170.93267 METERS 172.22304 METERS 1.7374398 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR= |

25 10.000 METERS 1.00 204.78753 METERS 203.25318 METERS 204.78753 METERS 1.4611400 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

29 10.000 METERS 1.00 237.35203 METERS 235.57368 METERS 237.35203 METERS 1.2606627 MM

33 10.000 METERS 1.00 269.91653 METERS 267.89419 METERS 1.1085623 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

37 10.000 METERS 1.00 302.48103 METERS 300.21470 METERS 302.48103 METERS 0.9892130 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

41 10.000 METERS 1.00 335.04552 METERS 332.53521 METERS 335.04552 METERS 0.8930649 MM

NO DE MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

45 10.000 METERS 1.00 367.61002 METERS 364.85572 METERS 367.61002 METERS 0.8139517 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR= -

49 10.000 METERS 1.00 400.17451 METERS 397.17622 METERS 400.17451 METERS 0.7477146 MM

53 10.000 METERS 1.00 432.73901 METERS 429.49673 METERS 432.73901 METERS 0.6914468 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

57 10.000 METERS 1.00 465.30350 METERS 461.81724 METERS 465.30350 METERS 0.6430549 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

61 10.000 METERS 1.00 497.86800 METERS 494.13775 METERS 497.86800 METERS 0.6009936 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

65 10.000 METERS 1.00 530.43250 METERS 526.45826 METERS 530.43250 METERS 0.5640968 MM

5 28.000 METERS 1.25 146.49014 METERS 116.62178 METERS 117.19212 METERS 16.0719399 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

9 28.000 METERS 1.25 260.16515 METERS 207.11920 METERS 208.13212 METERS 9.0466228 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

13 28.000 METERS 1.25 373.84015 METERS 297.61663 METERS 299.07212 METERS 6.2952936 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

17 28.000 METERS 1.25 487.51514 METERS 388.11405 METERS 390.01212 METERS 4.8272619 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

21 28.000 METERS 1.25 601.19014 METERS 478.61147 METERS 480.95211 METERS 3.9144506 MM

25 28,000 METERS 1.25 714.86514 METERS 569.10889 METERS 3.2919635 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= EDCAL LENGTH DE REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR FLECTRICAL DIAMETER= 662.83212 METERS SURFACE APPROXIMATION ERROR=

29 28.000 METERS 1.25 828.54015 METERS 659.60632 METERS 2.8402947 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 753.77211 METERS SURFACE APPROXIMATION ERROR=

33 28.000 METERS 1.25 942.21514 METERS 750.10374 METERS 2.4976147 MM

NO DE MODULES ACROSS CORNERS= -MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= 840.60117 METERS REFLECTOR ELECTRICAL DIAMETER= 844.71212 METERS SURFACE APPROXIMATION ERROR=

37 28.000 METERS 1.25 -1055.89015 METERS 2.2287214 MM

NO OF MODULES ACROSS CORMERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 935.65211 METERS SURFACE APPROXIMATION ERROR=

28.000 METERS 1.25 1169.56514 METERS 931.09859 METERS 2.0120992 MM

NO OF MODULES ACROSS CORNERS= 45
MODULE DIAMETER ACROSS CORNERS= 28.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 1.25
FOCAL LENGTH OF REFLECTOR= 1283.24014 METERS
REFLECTOR PHYSICAL DIAMETER= 1021.59602 METERS
REFLECTOR ELECTRICAL DIAMETER= 1026.59212 METERS
SURFACE APPROXIMATION ERROR= 1.8338564 MM

MODULE DIAMETER ACROSS CORNERS= 49

MODULE DIAMETER ACROSS CORNERS= 28.000 METERS

FOCAL LENGTH TO DIAMETER RATIO= 1.25

FOCAL LENGTH OF REFLECTOR= 1396.91513 METERS

REFLECTOR PHYSICAL DIAMETER= 1112.09343 METERS

REFLECTOR ELECTRICAL DIAMETER= 1117.53210 METERS

SURFACE APPROXIMATION ERROR= 1.6846234 MM

NO OF MODULES ACROSS CORNERS= 53

MODULE DIAMETER ACROSS CORNERS= 28.000 METERS

FOCAL LENGTH TO DIAMETER RATIO= 1.25

FOCAL LENGTH OF REFLECTOR= 1510.59013 METERS

REFLECTOR PHYSICAL DIAMETER= 1202.59085 METERS

REFLECTOR ELECTRICAL DIAMETER= 1208.47211 METERS

SURFACE APPROXIMATION ERROR= 1.5578509 MM

NO OF MODULES ACROSS CORNERS= 57

MODULE DIAMETER ACROSS CORNERS= 28.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 1.25

FOCAL LENGTH OF REFLECTOR= 1624.26514 METERS
REFLECTOR PHYSICAL DIAMETER= 1293.08827 METERS
REFLECTOR ELECTRICAL DIAMETER= 1299.41211 METERS
SURFACE APPROXIMATION ERROR= 1.4488231 MM

NO OF MODULES ACROSS CORNERS= 61

MODULE DIAMETER ACROSS CORNERS= 28.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 1.25

FOCAL LENGTH OF REFLECTOR= 1737.94014 METERS
REFLECTOR PHYSICAL DIAMETER= 1383.58569 METERS
REFLECTOR ELECTRICAL DIAMETER= 1390.35211 METERS
SURFACE APPROXIMATION ERROR= 1.3540580 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= -28.000 METERS EDCAL LENGTH TO DIAMETER RATIO= 1.25 FOCAL LENGTH OF REFLECTOR= 1851.61514 METERS REFLECTOR PHYSICAL DIAMETER= 1474.08313 METERS REFLECTOR ELECTRICAL DIAMETER= 1481.29211 METERS SURFACE APPROXIMATION FRACE -1.2709287 MM

NO DE MODULES ACROSS CORNERS= -MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

5 22.000 METERS 1.25 115,09940 METERS 91.63140 METERS 92.07952 METERS 12.6279528 MM

NO DE MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 163.53238 METERS SURFACE APPROXIMATION ERROR=

22.000 METERS 1.25 204.41547 METERS 162.73652 METERS 7.1080608 MM

NO DE MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 234.98524 METERS SURFACE APPROXIMATION ERROR=

13 22.000 METERS 1.25 293.73154 METERS 233.84163 METERS 4.9463022 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= | FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

17 22.000 METERS 1.25 383.04762 METERS 304,94675 METERS 306.43809 METERS 3.7928486 MM

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21 22.000 METERS 1.25 472.36368 METERS 376.05187 METERS 377.89095 METERS 3.0756398 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 449.34380 METERS SURFACE APPROXIMATION ERROR=

25 22.000 METERS 1.25 561.67976 METERS 447.15699 METERS 2.5865428 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

29 22.000 METERS 1.25 650.99583 METERS 518.26211 METERS 520.79666 METERS 2.2316601 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= -SURFACE APPROXIMATION ERROR=

33 22.000 METERS 1.25 740.31190 METERS 589.36723 METERS 592.24952 METERS 1.9624115 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= -SUPFACE APPROXIMATION ERROR=

37 22.000 METERS 1.25 829.62798 METERS 660.47234 METERS 663.70238 METERS 1.7511382 MM

41 22.000 METERS 1.25 918.94405 METERS 731.57746 METERS 735.15524 METERS 1.5809351 MM

45

NO OF MODULES ACROSS CORNERS= 22.000 METERS MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= 1.25 FOCAL LENGTH OF REFLECTOR= -1008.26012 METERS REFLECTOR PHYSICAL DIAMETER= | 802.68258 METERS REFLECTOR ELECTRICAL DIAMETER= 806.60809 METERS 1.4408872 MM SURFACE APPROXIMATION ERROR= |

NO OF MODULES ACROSS CORNERS= 49 MODULE DIAMETER ACROSS CORNERS= 22.000 METERS FOCAL LENGTH TO DIAMETER RATIO= 1.25 FOCAL LENGTH OF REFLECTOR= 1097.57617 METERS REFLECTOR PHYSICAL DIAMETER= 873.78769 METERS REFLECTOR ELECTRICAL DIAMETER= 878.06094 METERS SURFACE APPROXIMATION ERROR= 1.3236327 MM

NO OF MODULES ACROSS CORNERS= 53 MODULE DIAMETER ACROSS CORNERS= 22.000 METERS FOCAL LENGTH TO DIAMETER RATIO= 1.25 1186.89224 METERS FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= 944.89281 METERS REFLECTOR ELECTRICAL DIAMETER= 949.51379 METERS SURFACE APPROXIMATION ERROR= 1.2240257 MM

NO OF MODULES ACROSS CORNERS= 57 MODULE DIAMETER ACROSS CORNERS= 22.000 METERS FOCAL LENGTH TO DIAMETER RATIO= 1.25 FOCAL LENGTH OF REFLECTOR= 1276.20833 METERS 1015.99793 METERS REFLECTOR PHYSICAL DIAMETER= | REFLECTOR ELECTRICAL DIAMETER= 1020.96666 METERS SURFACE APPROXIMATION ERROR= 1.1383610 MM

NO OF MODULES ACROSS CORNERS= 61 MODULE DIAMETER ACROSS CORNERS= 22.000 METERS FOCAL LENGTH TO DIAMETER RATIO= 1.25 FOCAL LENGTH OF REFLECTOR= 1365.52438 METERS REFLECTOR PHYSICAL DIAMETER= 1087.10304 METERS REFLECTOR ELECTRICAL DIAMETER= 1092.41951 METERS SURFACE APPROXIMATION FRROR= -1.0639027 MM

NO OF MODULES ACROSS CORNERS= 65 MODULE DIAMETER ACROSS CORNERS= 22.000 METERS FOCAL LENGTH TO DIAMETER RATIO= 1.25 FOCAL LENGTH OF REFLECTOR= 1454.84047 METERS REFLECTOR PHYSICAL DIAMETER= 1158.20818 METERS REFLECTOR ELECTRICAL DIAMETER= 1163.87238 METERS SURFACE APPROXIMATION ERROR= 0.9985868 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

16.000 METERS 1.25 83.70865 METERS 66.64102 METERS 66.96692 METERS 9.1839657 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 118.93264 METERS SURFACE APPROXIMATION ERROR=

16.000 METERS 1.25 148.66580 METERS 118.35383 METERS 5.1694989 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 170.89835 METERS SURFACE APPROXIMATION ERROR=

13 16.000 METERS 1.25 213.62294 METERS 170.06664 METERS 3.5973107 MM

NO DE MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= EDCAL LENGTH ID DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETERS 222.86407 METERS SURFACE APPROXIMATION ERROR=

17 16.000 METERS 1.25 278.58008 METERS 221.77946 METERS 2.7584354 MM

NO DE MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION FRROR=

21 16.000 METERS 1.25 343.53723 METERS 273.49227 METERS 274_82978 METERS 2.2368289 MM

NO DE MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER≈ 326.79549 METERS SURFACE APPROXIMATION ERROR=

25 16.000 METERS 1.25 408.49437 METERS 325.20508 METERS 1.8811220 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 378.76121 METERS SURFACE APPROXIMATION ERROR=

29 16.000 METERS 1.25 473.45151 METERS 376.91790 METERS 1.6230255 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

33 16.000 METERS 1.25 538.40865 METERS 428.63071 METERS 430.72692 METERS 1.4272084 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

37 16.000 METERS 1.25 603.36579 METERS 480.34352 METERS 482.69263 METERS 1.2735551 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

41 16.000 METERS 1.25 668.32294 METERS 532.05634 METERS 534.65835 METERS 1.1497710 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

45 16.000 METERS 1.25 733.28009 METERS 583.76915 METERS 586.62407 METERS 1.0479179 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

49 16.000 METERS 1.25 798.23722 METERS 635.48196 METERS 638.58978 METERS 0.9626420 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERPOR=

53 16.000 METERS 1.25 863.19436 METERS 687.19477 METERS 690.55549 METERS 0.8902005 MM MO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

57 16.000 METERS 1.25 928.15150 METERS 738.90759 METERS 742.52120 METERS 0.8278989 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

61 16.000 METERS 1.25 993.10866 METERS 790.62040 METERS 794.48692 METERS 0.7737474 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR= 1
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

65 16.000 METERS 1.25 1058.06580 METERS 842.33321 METERS 846.45264 METERS 0.7262450 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

5 10.000 METERS 1.25 52.31791 METERS 41.65064 METERS 41.85433 METERS 5.7399784 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

9 10.000 METERS 1.25 92.91612 METERS 73.97114 METERS 74.33290 METERS 3.2309367 MM NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 106.81147 METERS SURFACE APPROXIMATION ERROR=

13 10.000 METERS 1.25 133.51434 METERS 106.29165 METERS 2.2483192 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

17 10.000 METERS 1.25 174.11255 METERS 138.61216 METERS 139.29004 METERS 1.7240221 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 171.76861 METERS SURFACE APPROXIMATION ERROR=

21 10.000 METERS 1.25 214.71077 METERS 170.93267 METERS 1.3980180 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 204.24718 METERS SURFACE APPROXIMATION FRACE

25 10.000 METERS 1.25 255.30898 METERS 203.25318 METERS 1.1757012 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

29 10.000 METERS 1.25 295.90720 METERS 235.57368 METERS 236.72576 METERS 1.0143909 MM

NO OF MODULES ACROSS CORNERS=
MODULE BIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

33 10.000 METERS 1.25 336.50541 METERS 267.89419 METERS 269.20433 METERS 0.8920052 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

37 10.000 METERS 1.25 377.10363 METERS 300.21470 METERS 301.68290 METERS 0.7959719 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

41 10.000 METERS 1.25 417.70184 METERS 332.53521 METERS 334.16147 METERS 0.7186068 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

45 10.000 METERS 1.25 458.30006 METERS 364.85572 METERS 366.64005 METERS 0.6549487 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

49 10.000 METERS 1.25 498.89826 METERS 397.17622 METERS 399.11861 METERS 0.6016512 MM NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= EDCAL LENGTH DE REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 431.59718 METERS SURFACE APPROXIMATION ERROR=

53 10.000 METERS 1.25 539,49648 METERS 429.49673 METERS 0.5563753 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 464.07576 METERS SURFACE APPROXIMATION ERROR=

10.000 METERS 1.25 580.09470 METERS 461.81724 METERS 0.5174368 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 496.55433 METERS SURFACE APPROXIMATION FRROR=

61 10.000 METERS 1.25 620.69291 METERS 494.13775 METERS 0.4835921 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 529.03290 METERS SURFACE APPROXIMATION ERROR=

65 10.000 METERS 1.25 661.29112 METERS 526.45826 METERS 0.4539031 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= | FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 117.02051 METERS SURFACE APPROXIMATION ERROR=

5 28.000 METERS 1.50 175.53076 METERS 116.62178 METERS 13.4331638 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 207.82734 METERS SURFACE APPROXIMATION ERROR=

28.000 METERS 1.50 311.74100 METERS 207.11920 METERS 7.5620744 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

13 28.000 METERS 1.50 447.95126 METERS 297.61663 METERS 298.63417 METERS 5.2623661 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

17 28.000 METERS 1.50 584.16151 METERS 388.11405 METERS 389.44100 METERS 4.0352458 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 480.24783 METERS SURFACE APPROXIMATION ERROR=

21 28.000 METERS 1.50 720.37175 METERS 478.61147 METERS 3.2722159 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

25 28.000 METERS 1.50 856.58200 METERS 569.10889 METERS 571.05466 METERS 2.7518658 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

29 28.000 METERS 1.50 992.79224 METERS 659.60632 METERS 661.86150 METERS 2.3743040 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR= 1
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

33 : 28.000 METERS : 1.50 1129.00249 METERS 750.10374 METERS 752.66833 METERS 2.0878477 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR= 1
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

37 28.000 METERS 1.50 1265.21275 METERS 840.60117 METERS 843.47517 METERS 1.8630713 MM

NO OF MODULES ACROSS CORNERS= 41

MODULE DIAMETER ACROSS CORNERS= 28.000 METERS

FOCAL LENGTH TO DIAMETER RATIO= 1.50

FOCAL LENGTH OF REFLECTOR= 1401.42299 METERS

REFLECTOR PHYSICAL DIAMETER= 931.09859 METERS

REFLECTOR ELECTRICAL DIAMETER= 934.28199 METERS

SUPFACE APPROXIMATION ERROR= 1.6819896 MM

MO OF MODULES ACROSS CORNERS= 45
MODULE DIAMETER ACROSS CORNERS= 28.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 1.50
FOCAL LENGTH OF REFLECTOR= 1537.63326 METERS
REFLECTOR PHYSICAL DIAMETER= 1021.59602 METERS
REFLECTOR ELECTRICAL DIAMETER= 1025.08884 METERS
SURFACE APPROXIMATION ERROR= 1.5329903 MM

NO OF MODULES ACROSS CORNERS= 49
MODULE DIAMETER ACROSS CORNERS= 28.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 1.50
FOCAL LENGTH OF REFLECTOR= 1673.84349 METERS
REFLECTOR PHYSICAL DIAMETER= 1112.09343 METERS
REFLECTOR ELECTRICAL DIAMETER= 1115.89566 METERS
SURFACE APPROXIMATION ERROR= 1.4082412 MM

NO OF MODULES ACROSS CORNERS= 53
MODULE DIAMETER ACROSS CORNERS= 28.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 1.50
FOCAL LENGTH OF REFLECTOR= 1810.05373 METERS
REFLECTOR PHYSICAL DIAMETER= 1202.59085 METERS
REFLECTOR ELECTRICAL DIAMETER= 1206.70248 METERS
SURFACE APPROXIMATION ERROR= 1.3022675 MM

NO OF MODULES ACROSS CORNERS= 57

MODULE DIAMETER ACROSS CORNERS= 28.000 METERS
FOCAL LENGTH OF REFLECTOR= 1.50

FOCAL LENGTH OF REFLECTOR= 1946.26396 METERS
REFLECTOR PHYSICAL DIAMETER= 1293.08827 METERS
REFLECTOR ELECTRICAL DIAMETER= 1297.50931 METERS
SURFACE APPROXIMATION ERROR= 1.2111272 MM

NO OF MODULES ACROSS CORNERS= 61
MODULE DIAMETER ACROSS CORNERS= 28.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 1.50
FOCAL LENGTH OF REFLECTOR= 2082.47421 METERS
REFLECTOR PHYSICAL DIAMETER= 1383.58569 METERS
REFLECTOR ELECTRICAL DIAMETER= 1388.31615 METERS
SURFACE APPROXIMATION ERROR= 1.1319095 MM

NO OF MODULES ACROSS CORNERS= 65 MODULE DIAMETER ACROSS CORNERS= 28.000 METERS FOCAL LENGTH TO DIAMETER RATIO= 1.50 FOCAL LENGTH OF REFLECTOR= 2218.68448 METERS REFLECTOR PHYSICAL DIAMETER= 1474.08313 METERS REFLECTOR ELECTRICAL DIAMETER≈ 1479.12299 METERS SURFACE APPROXIMATION ERROR= -1.0624187 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

5 22.000 METERS 1.50 137.91702 METERS 91.63140 METERS 91.94468 METERS 10.5546287 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

9 22.000 METERS 1.50 244.93936 METERS 162.73652 METERS 163.29291 METERS 5.9416299 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 234.64113 METERS SURFACE APPROXIMATION ERROR=

13 22.000 METERS 1.50 351.96170 METERS 233.84163 METERS 4.1347162 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 305.98936 METERS SURFACE APPROXIMATION ERROR=

17 22.000 METERS 1.50 458.98404 METERS 304.94675 METERS 3.1705504 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 377.33758 METERS SURFACE APPROXIMATION ERROR=

21 22.000 METERS 1.50 566.00637 METERS 376.05187 METERS 2.5710268 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 448.68581 METERS SURFACE APPROXIMATION ERROR=

25 22.000 METERS 1.50 673.02871 METERS 447.15699 METERS 2.1621803 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= | FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SHREACE APPROXIMATION ERROR=

29 22.000 METERS 1.50 780.05106 METERS 518.26211 METERS 520.03403 METERS 1.8655246 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

33 22.000 METERS 1.50 887.07339 METERS 589.36723 METERS 591.38226 METERS 1.6404518 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 662.73048 METERS SURFACE APPROXIMATION ERROR=

37 22.000 METERS 1.50 994.09573 METERS 660.47234 METERS 1.4638418 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER, RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

41
22.000 METERS
1.50
1101.11807 METERS
731.57746 METERS
734.07871 METERS

NO OF MODULES ACROSS CORNERS= 45

MODULE DIAMETER ACROSS CORNERS= 22.000 METERS

FOCAL LENGTH TO DIAMETER RATIO= 1.50

FOCAL LENGTH OF REFLECTOR= 1208.14040 METERS

REFLECTOR PHYSICAL DIAMETER= 802.68258 METERS

REFLECTOR ELECTRICAL DIAMETER= 805.42693 METERS

SURFACE APPROXIMATION ERROR= 1.2044924 MM

NO OF MODULES ACROSS CORNERS= 49

MODULE DIAMETER ACROSS CORNERS= 22.000 METERS

FOCAL LENGTH TO DIAMETER RATIO= 1.50

FOCAL LENGTH OF REFLECTOR= 1315.16274 METERS

REFLECTOR PHYSICAL DIAMETER= 873.78769 METERS

REFLECTOR ELECTRICAL DIAMETER= 876.77515 METERS

SURFACE APPROXIMATION ERROR= 1.1064752 MM

NO OF MODULES ACROSS CORNERS= 53

MODULE DIAMETER ACROSS CORNERS= 22.000 METERS

FOCAL LENGTH TO DIAMETER RATIO= 1.50

FOCAL LENGTH OF REFLECTOR= 1422.18506 METERS

REFLECTOR PHYSICAL DIAMETER= 944.89281 METERS

REFLECTOR ELECTRICAL DIAMETER= 948.12337 METERS

SURFACE APPROXIMATION ERROR= 1.0232102 MM

NO OF MODULES ACROSS CORNERS= 57

MODULE DIAMETER ACROSS CORNERS= 22.000 METERS

FOCAL LENGTH TO DIAMETER RATIO= 1.50

FOCAL LENGTH OF REFLECTOR= 1529.20741 METERS

REFLECTOR PHYSICAL DIAMETER= 1015.99793 METERS

REFLECTOR ELECTRICAL DIAMETER= 1019.47161 METERS

SURFACE APPROXIMATION ERROR= 0.9515999 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= 22.000 METERS FOCAL LEMGTH TO DIAMETER RATIO= 1.50 FOCAL LENGTH OF REFLECTOR= 1636.22974 METERS REFLECTOR PHYSICAL DIAMETER= 1087.10304 METERS REFLECTOR ELECTRICAL DIAMETER= 1090.81982 METERS SURFACE APPROXIMATION ERROR= 0.8893575 MM

NO OF MODULES ACROSS CORNERS= -MODULE DIAMETER ACROSS CORNERS= 22.000 METERS FOCAL LEMGTH TO DIAMETER RATIO= 1.50 FOCAL LENGTH OF REFLECTOR= 1743.25209 METERS REFLECTOR PHYSICAL DIAMETER= 1158.20818 METERS REFLECTOR ELECTRICAL DIAMETER= 1162.16806 METERS SURFACE APPROXIMATION ERROR= 0.8347575 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 66.86886 METERS SURFACE APPROXIMATION ERROR=

16.000 METERS 1.50 -100.30329 METERS - 66.64102 METERS 7.6760936 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= 118.35383 METERS REFLECTOR ELECTRICAL DIAMETER= 118.75848 METERS SURFACE APPROXIMATION ERROR=

16.000 METERS 1.50178.13772 METERS 4.3211854 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= -FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 170.64810 METERS SURFACE APPROXIMATION ERROR=

13 16.000 METERS: 1.50 255.97215 METERS 170.06664 METERS 3.0070663 MM

NO OF MODULES ACROSS CORNERS= 1 MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 222.53771 METERS SURFACE APPROXIMATION ERROR=

17 16.000 METERS 1.50 333.80657 METERS 221.77946 METERS 2.3058548 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 274.42733 METERS SURFACE APPROXIMATION ERROR=

21 16.000 METERS 1.50 411.64100 METERS 273.49227 METERS 1.8698376 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

25 16.000 METERS 1.50 489.47543 METERS 325.20508 METERS 326.31695 METERS 1.5724947 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

29 16.000 METERS 1.50 567.30985 METERS 376.91790 METERS 378.20657 METERS 1.3567452 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 430.09619 METERS SURFACE APPROXIMATION ERROR=

33 16.000 METERS 1.50 645.14428 METERS 428.63071 METERS 1.1930558 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 481.98581 METERS SURFACE APPROXIMATION ERROR=

37 16.000 METERS 1.50 722.97871 METERS: 480.34352 METERS 1.0646122 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

41 16.000 METERS 1.50 800.81314 METERS 532.05634 METERS 533.87543 METERS 0.9611369 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

45 16.000 METERS 1.50 878.64757 METERS 583.76915 METERS 585.76505 METERS 0.8759945 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

49 16.000 METERS 1.50 956.48199 METERS 635.48196 METERS 637.65466 METERS 0.8047093 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 689.54427 METERS SURFACE APPROXIMATION ERROR=

53 16.000 METERS 1.50 1034.31641 METERS 687.19477 METERS 0.7441529 MM

NO OF MODULES ACROSS CORNERS= 57

MODULE DIAMETER ACROSS CORNERS= 16.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 1.50

FOCAL LENGTH OF REFLECTOR= 1112.15083 METERS
REFLECTOR PHYSICAL DIAMETER= 738.90759 METERS
REFLECTOR ELECTRICAL DIAMETER= 741.43389 METERS
SURFACE APPROXIMATION ERROR= 0.6920727 MM

NO DF MODULES ACROSS CORNERS= 61
MODULE DIAMETER ACROSS CORNERS= 16.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 1.50
FOCAL LENGTH OF REFLECTOR= 1189.98528 METERS
REFLECTOR PHYSICAL DIAMETER= 790.62040 METERS
REFLECTOR ELECTRICAL DIAMETER= 793.32352 METERS
SURFACE APPROXIMATION ERROR= 0.6468055 MM

NO OF MODULES ACROSS CORNERS= 65
MODULE DIAMETER ACROSS CORNERS= 16.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 1.50
FOCAL LENGTH OF REFLECTOR= 1267.81970 METERS
REFLECTOR PHYSICAL DIAMETER= 842.33321 METERS
REFLECTOR ELECTRICAL DIAMETER= 845.21313 METERS
SURFACE APPROXIMATION ERROR= 0.6070964 MM

NO OF MODULES ACROSS CORNERS= 5
MODULE DIAMETER ACROSS CORNERS= 10.000 METERS
FOCAL LENGTH TO DIAMETER RATIO= 1.50
FOCAL LENGTH OF REFLECTOR= 62.68956 METERS
PEFLECTOR PHYSICAL DIAMETER= 41.65064 METERS
REFLECTOR ELECTRICAL DIAMETER= 41.79304 METERS
SURFACE APPROXIMATION ERROR= 4.7975584 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR= 1
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

9 10.000 METERS 1.50 111.33607 METERS 73.97114 METERS 74.22405 METERS 2.7007408 MM NO DE MODHLES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR FLECTRICAL DIAMETER= 106.65506 METERS SURFACE APPROXIMATION FRADR=

1.3 10-000 METERS 1.50 159.98259 METERS 106.29165 METERS 1.8794165 MM

NO DE MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= ECCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH DE REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 139.08607 METERS SURFACE APPROXIMATION FRROR= -

17 10.000 METERS 1.50 208.62911 METERS 138.61216 METERS 1.4411593 MM

NO DE MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH DE REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR FLECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

21 10,000 METERS 1.50 257,27562 METERS 170.93267 METERS 171.51708 METERS 1.1686485 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR=. REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 203.94809 METERS SURFACE APPROXIMATION ERROR=

25 10.000 METERS 1.50 305.92214 METERS 203,25318 METERS 0.9828092 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 236.37911 METERS SURFACE APPROXIMATION ERROR=

1 ________

29 10.000 METERS 1.50 354.56866 METERS 235.57368 METERS 0.8479657 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION FRADR=

33 10.000 METERS 1.50 403.21518 METERS 267.89419 METERS 268.81012 METERS 0.7456599 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

37 10.000 METERS 1.50 451.86170 METERS 300.21470 METERS 301.24113 METERS 0.6653826 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

41 10.000 METERS 1.50 500.50821 METERS 332.53521 METERS 333.67214 METERS 0.6007106 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= SURFACE APPROXIMATION ERROR=

45 10.000 METERS 1.50 549.15473 METERS 364.85572 METERS 366.10315 METERS 0.5474965 MM

NO OF MODULES ACROSS CORNERS= MODULE DIAMETER ACROSS CORNERS= FOCAL LENGTH TO DIAMETER RATIO= FOCAL LENGTH OF REFLECTOR= REFLECTOR PHYSICAL DIAMETER= REFLECTOR ELECTRICAL DIAMETER= 398.53416 METERS SURFACE APPROXIMATION EPROR=

49 10.000 METERS 1.50 597.80124 METERS 397.17622 METERS 0.5029433 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

53 10.000 METERS 1.50 646.44776 METERS 429.49673 METERS 430.96517 METERS 0.4650955 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

57 10.000 METERS 1.50 695.09428 METERS 461.81724 METERS 463.39619 METERS 0.4325454 MM

NO OF MODULES ACROSS CORNERS=
MODULE DIAMETER ACROSS CORNERS=
FOCAL LENGTH TO DIAMETER RATIO=
FOCAL LENGTH OF REFLECTOR=
REFLECTOR PHYSICAL DIAMETER=
REFLECTOR ELECTRICAL DIAMETER=
SURFACE APPROXIMATION ERROR=

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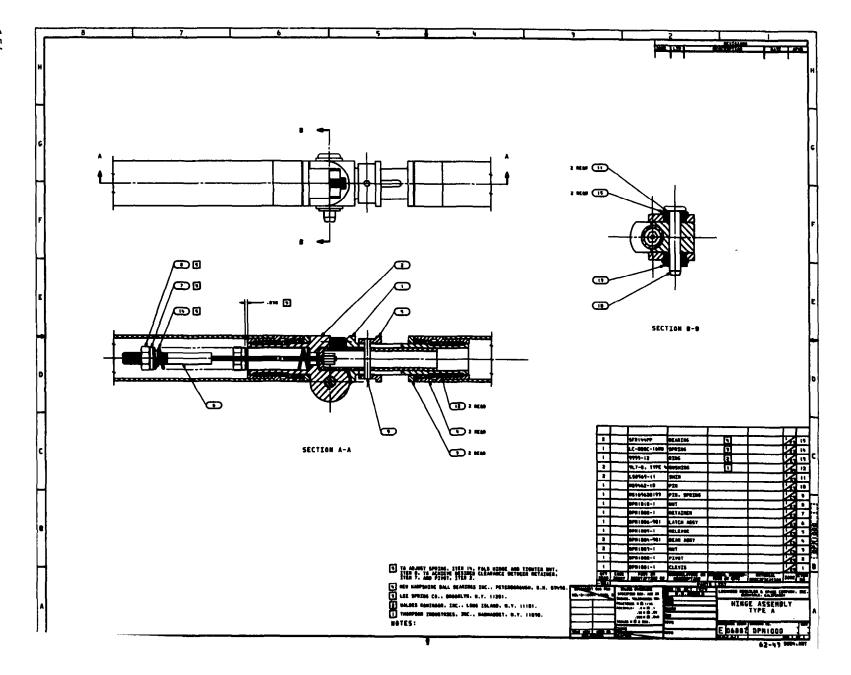
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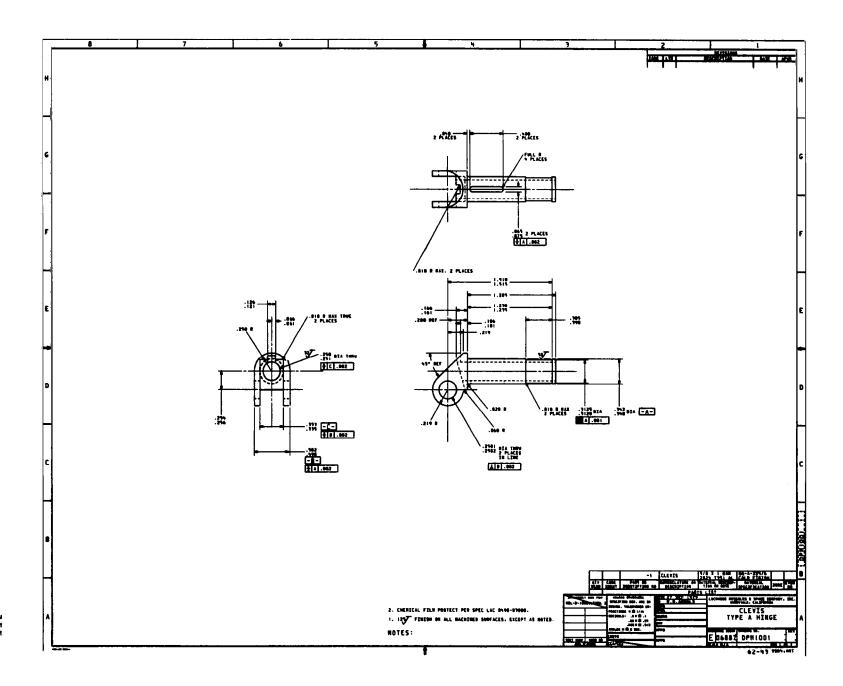
65 10.000 METERS 1.50 792.38731 METERS 526.45826 METERS 528.25821 METERS 0.3794352 MM

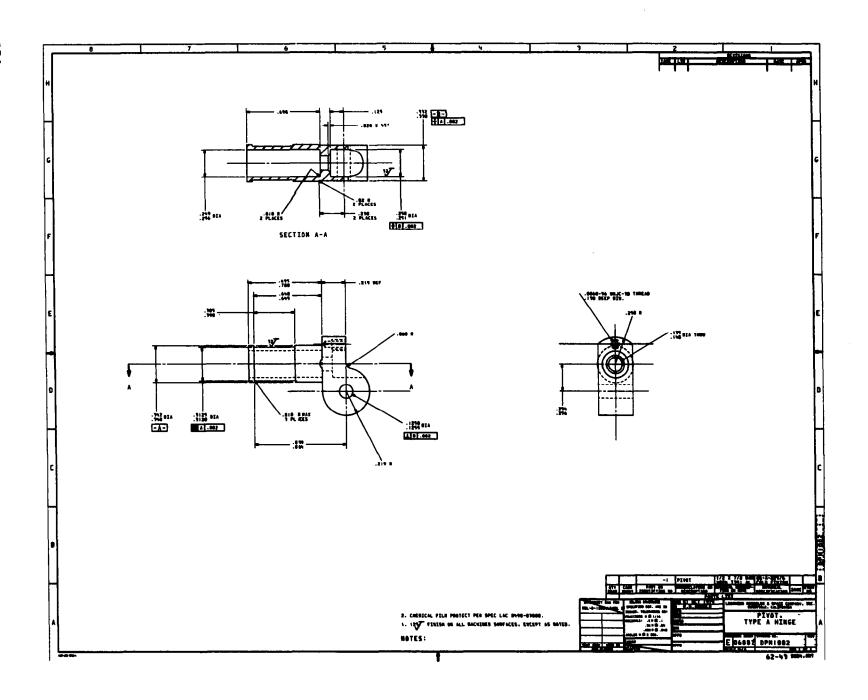
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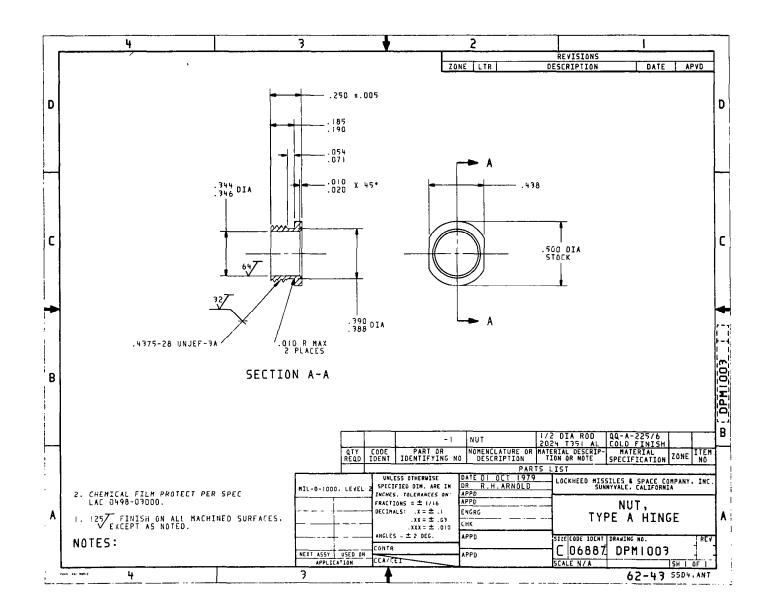
APPENDIX B

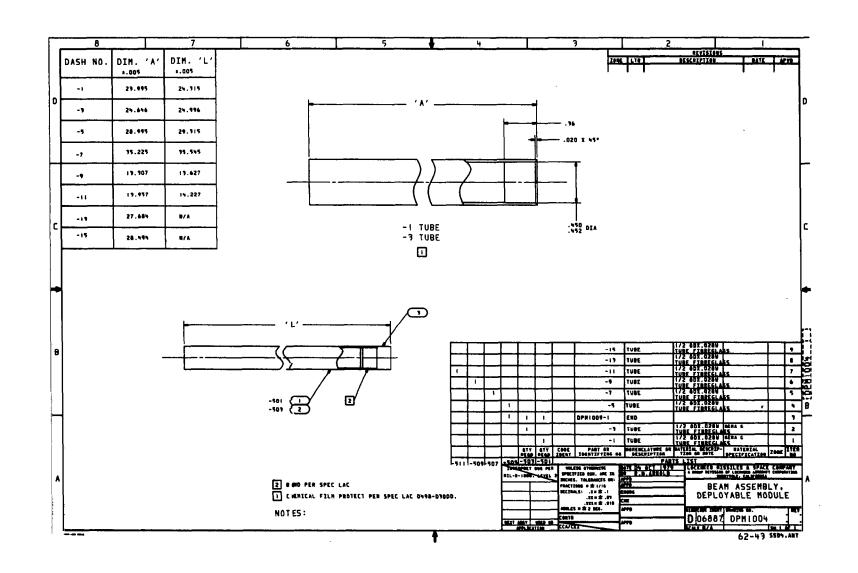
MODULAR ANTENNA MODEL DETAIL DRAWINGS

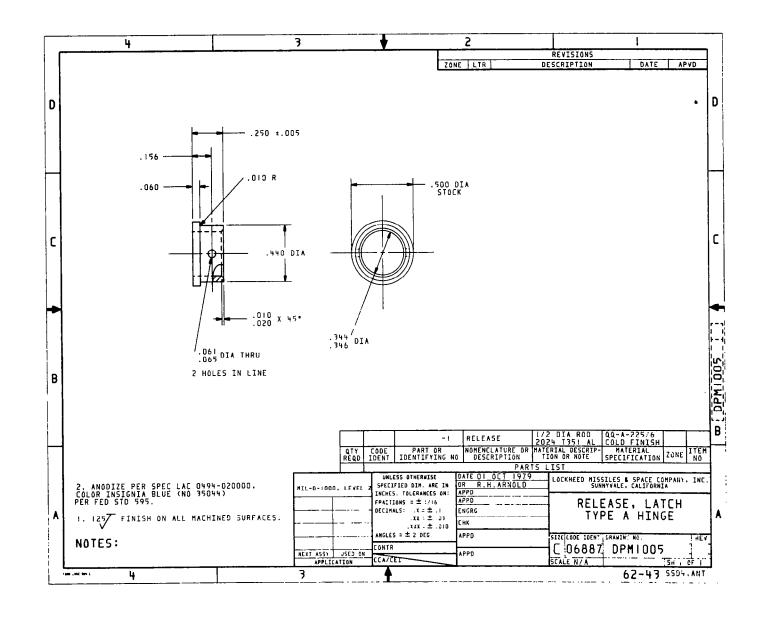


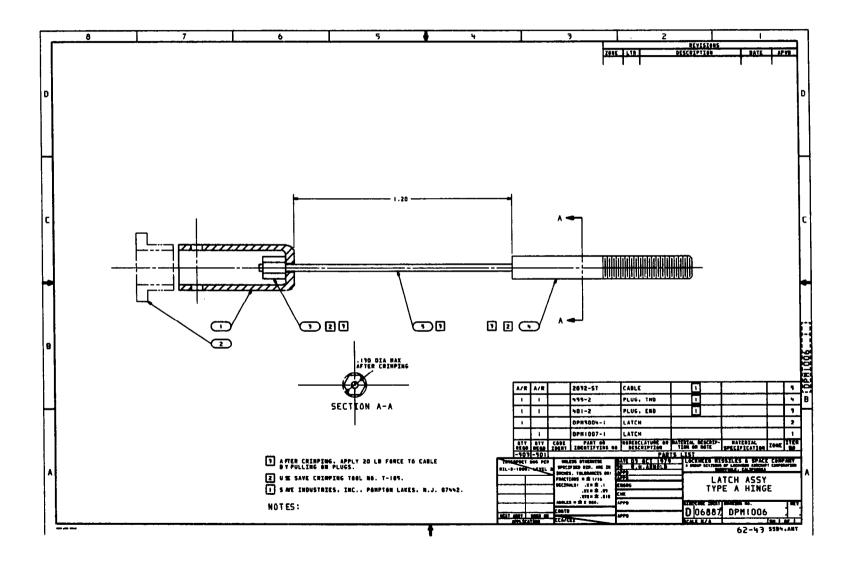


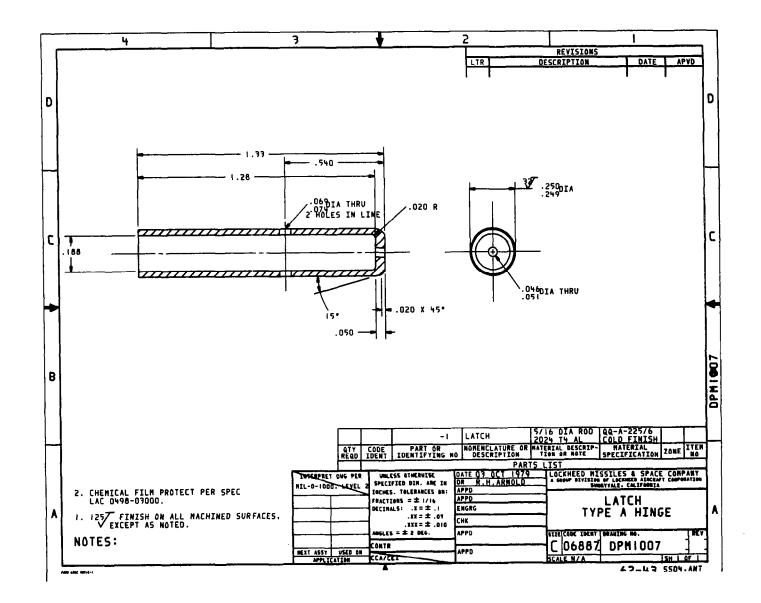


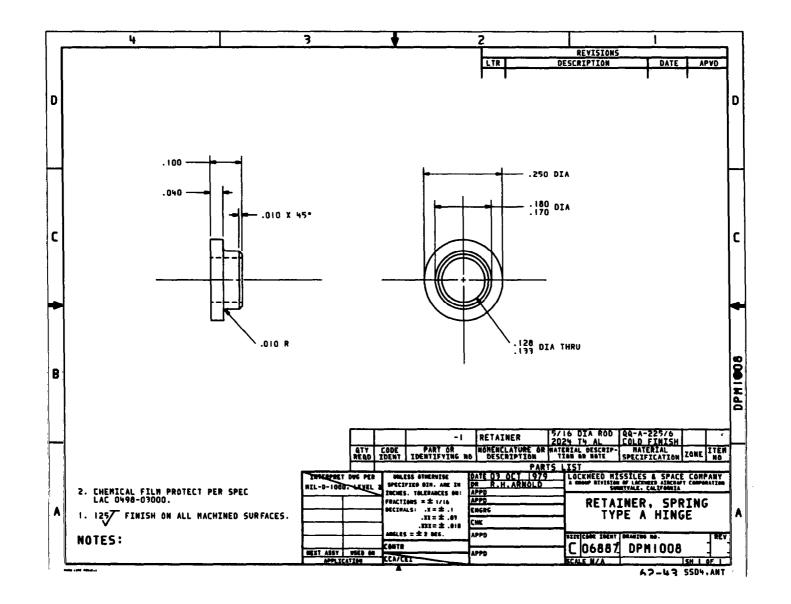


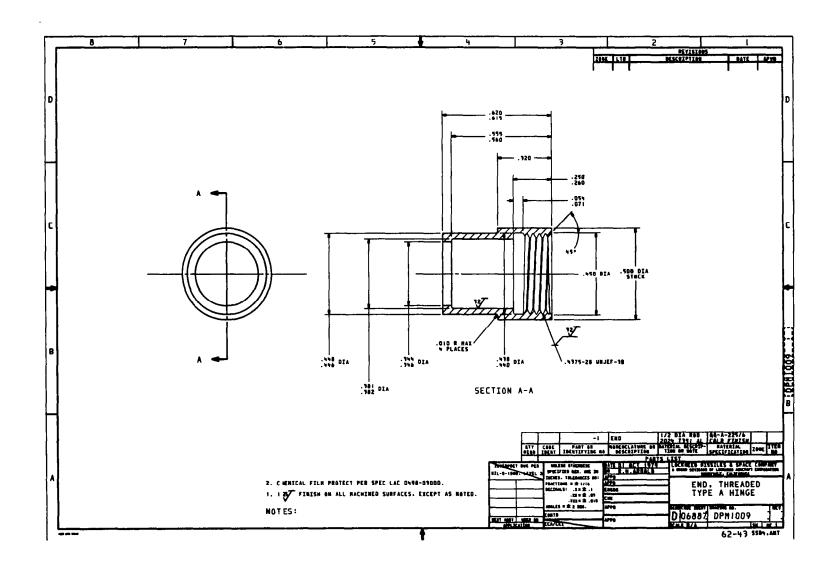


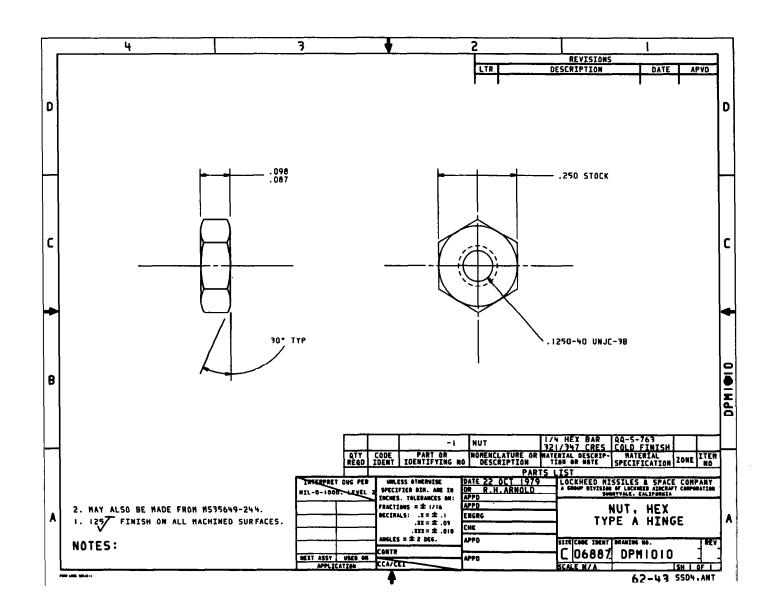


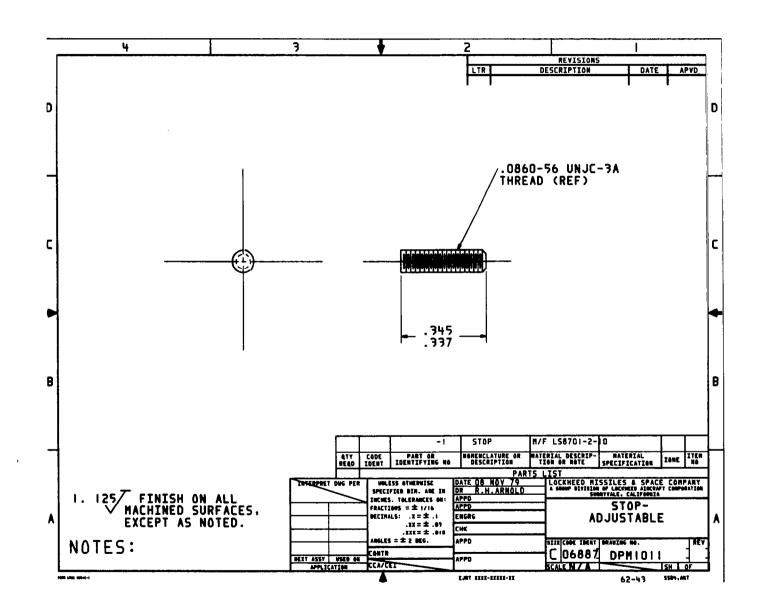


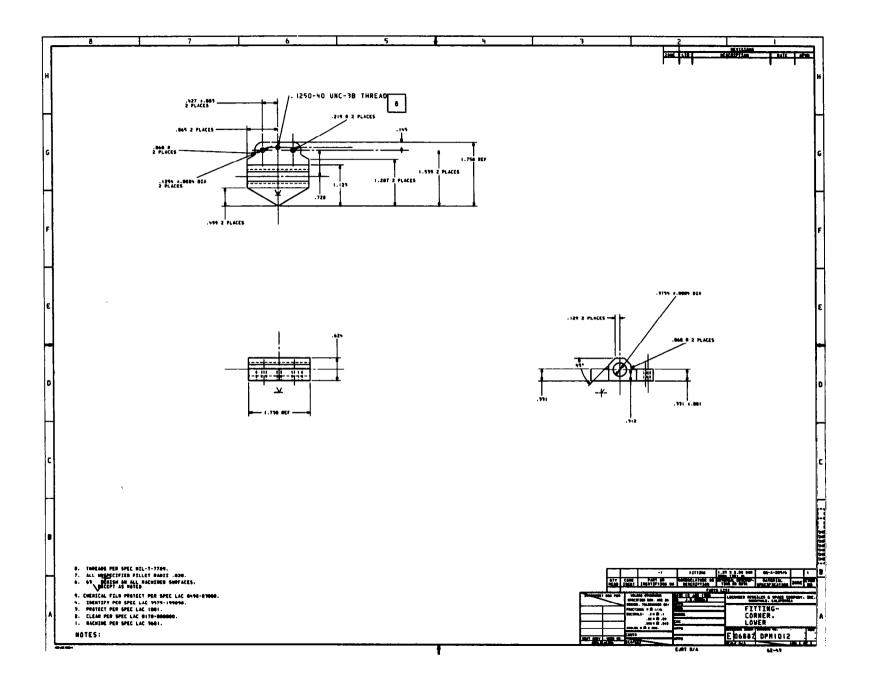


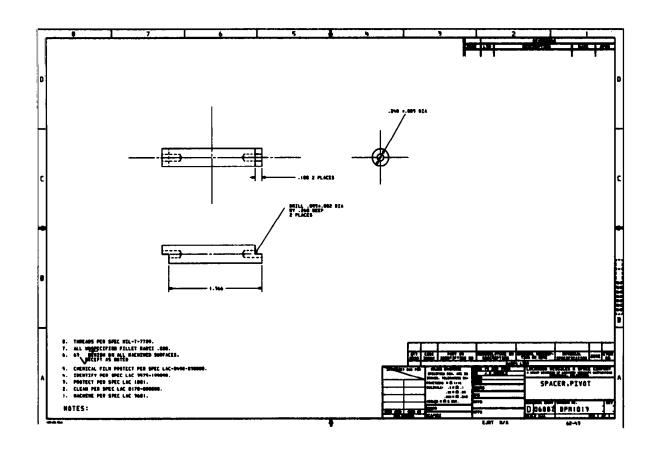


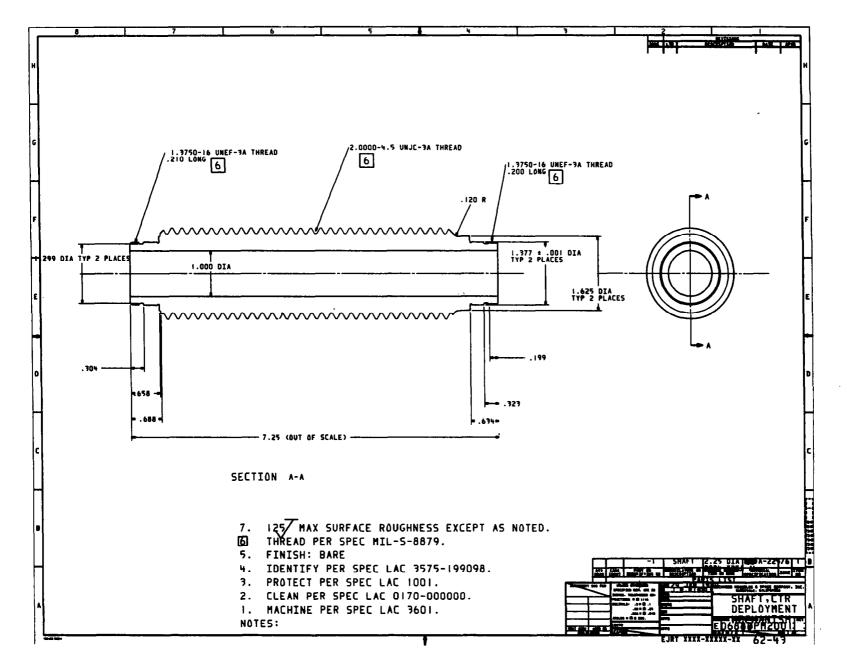


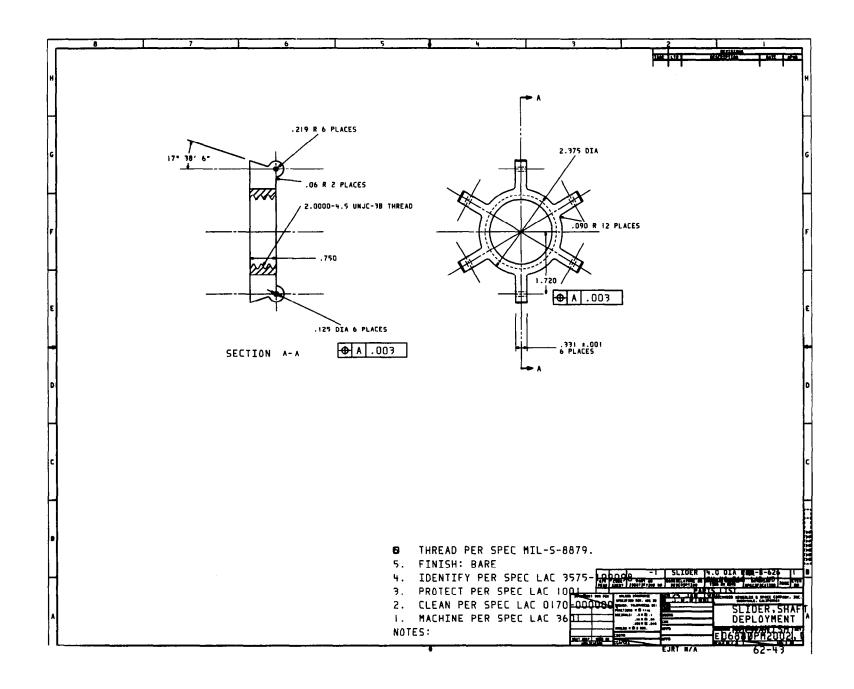


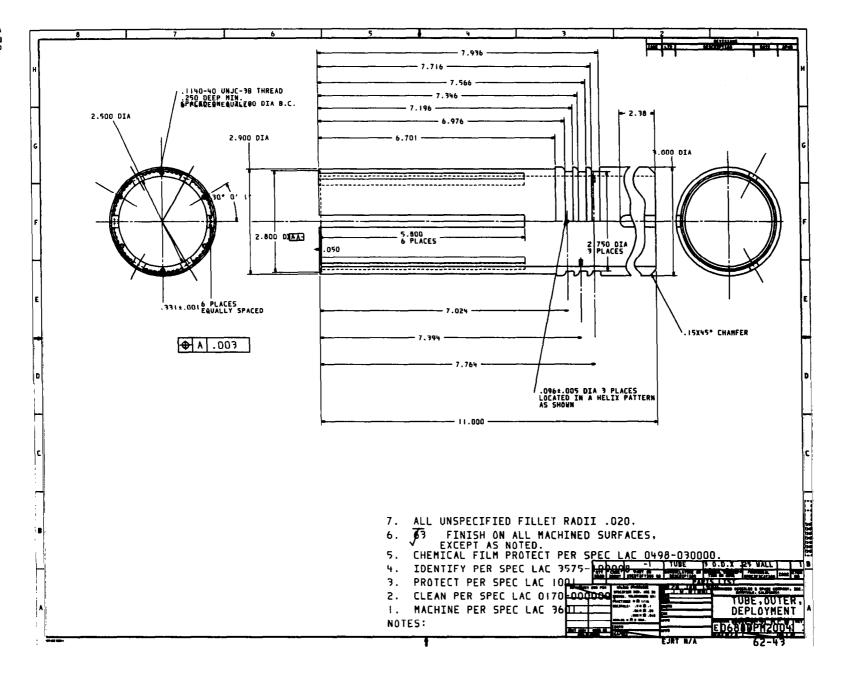


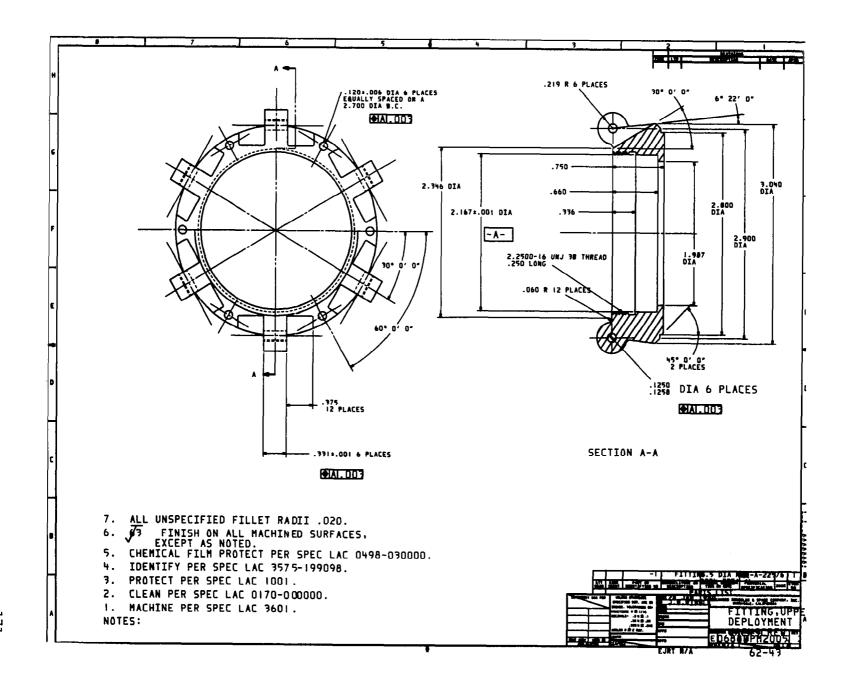


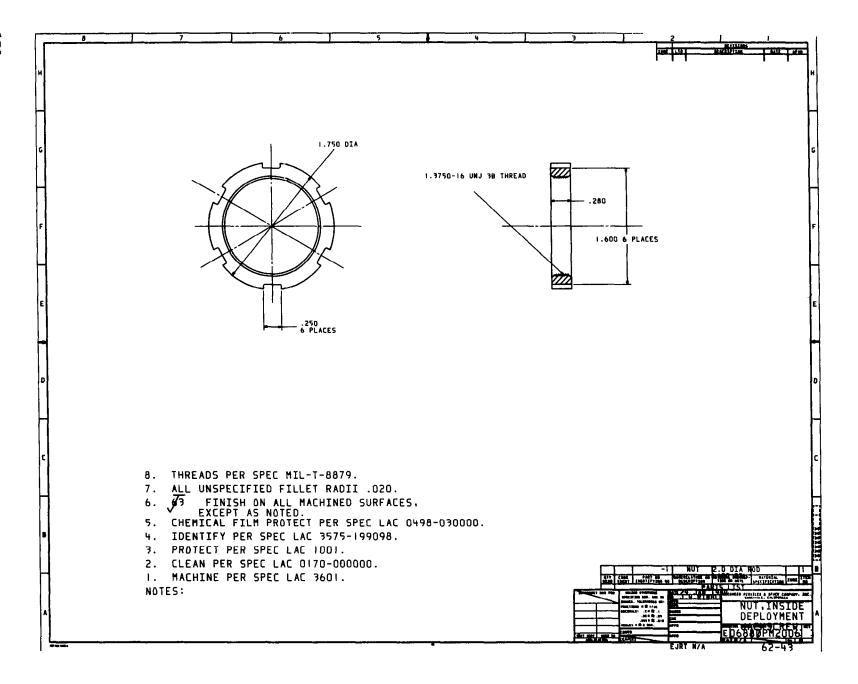


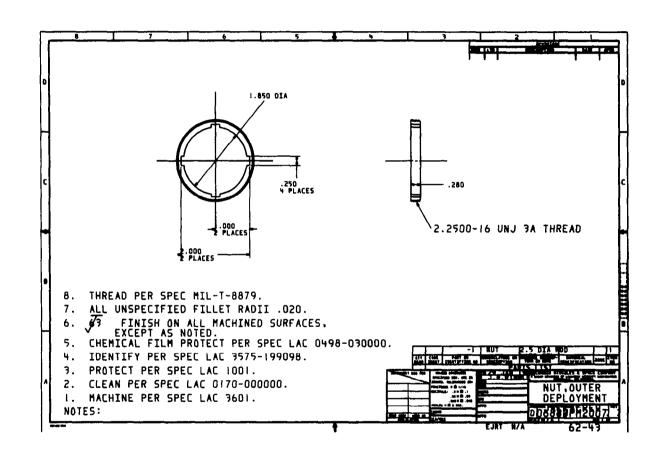


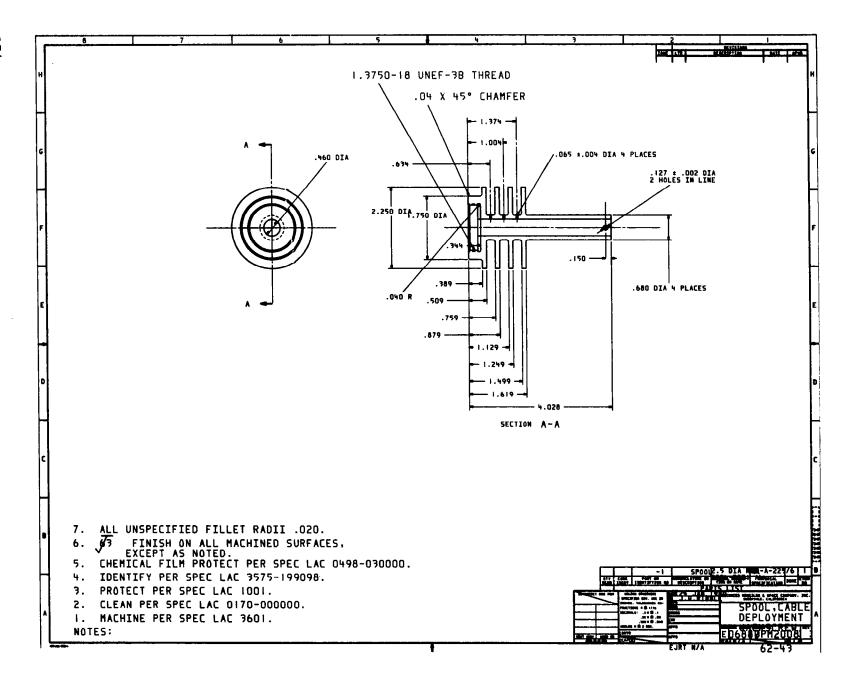


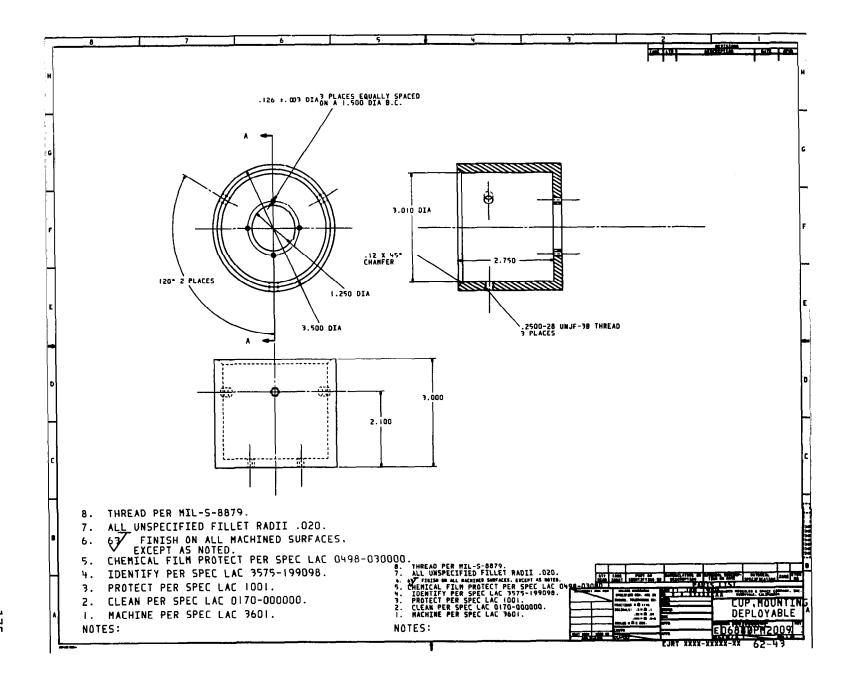


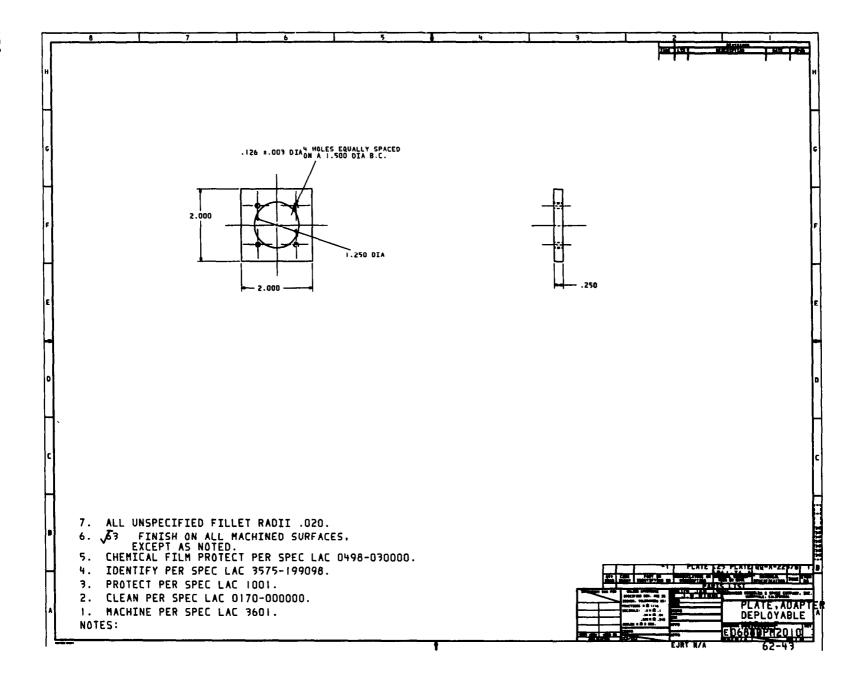


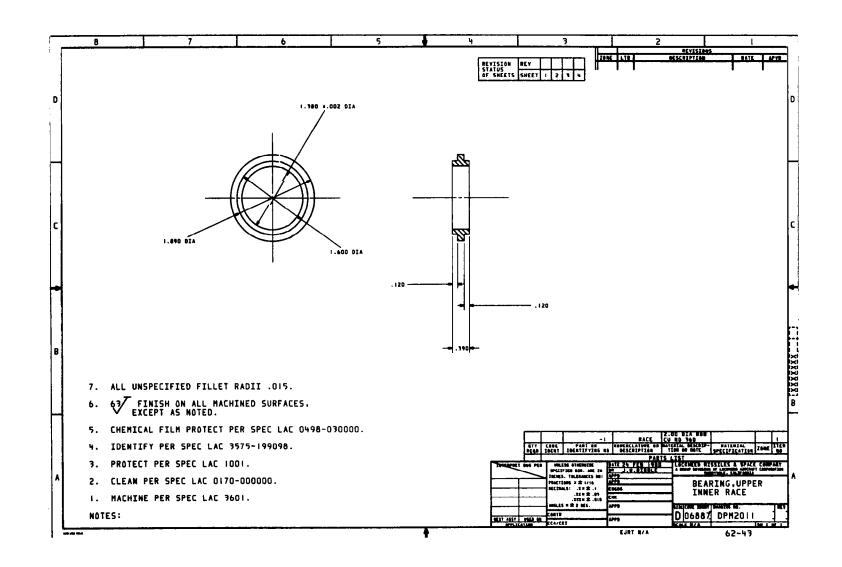


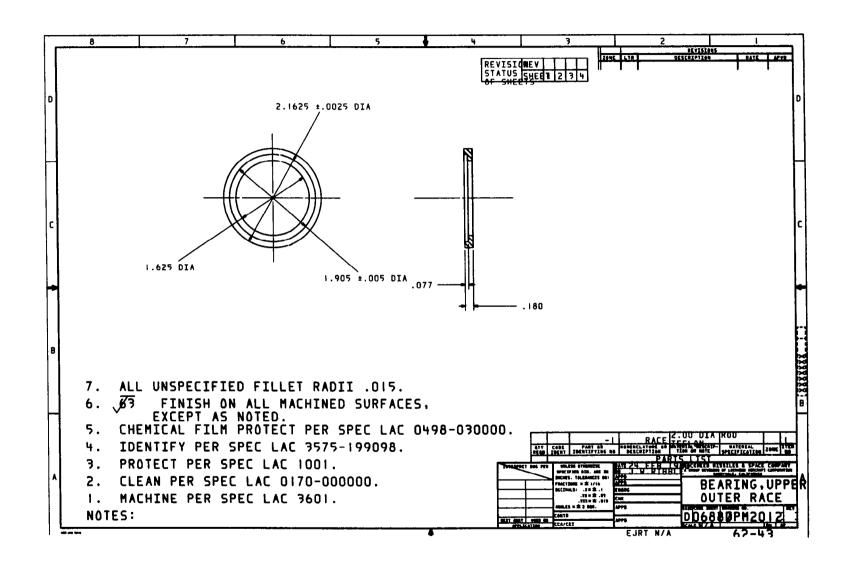


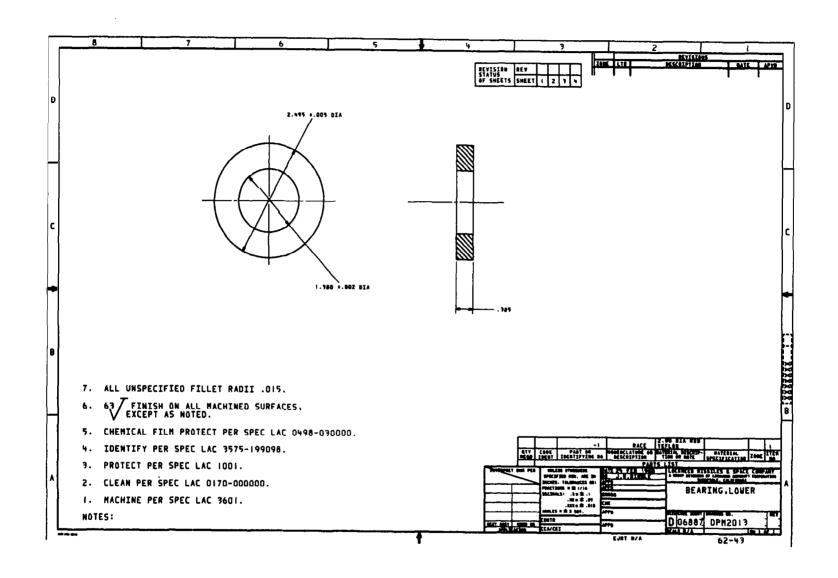


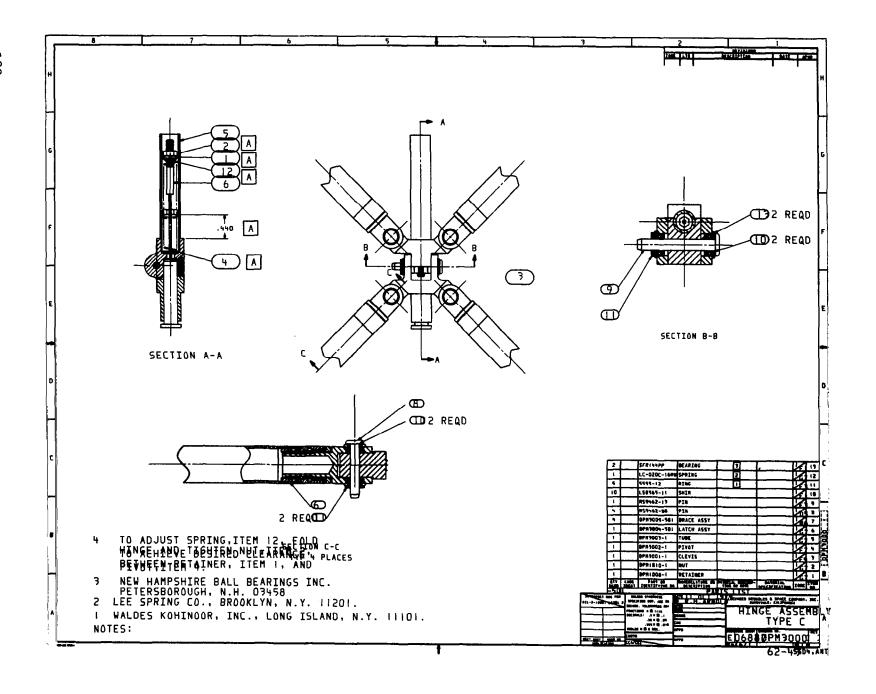


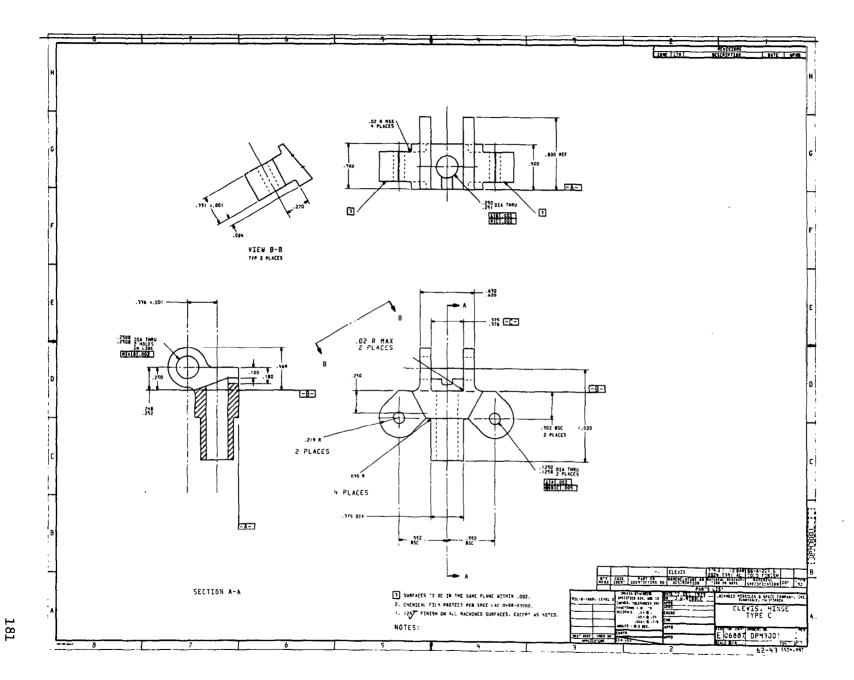


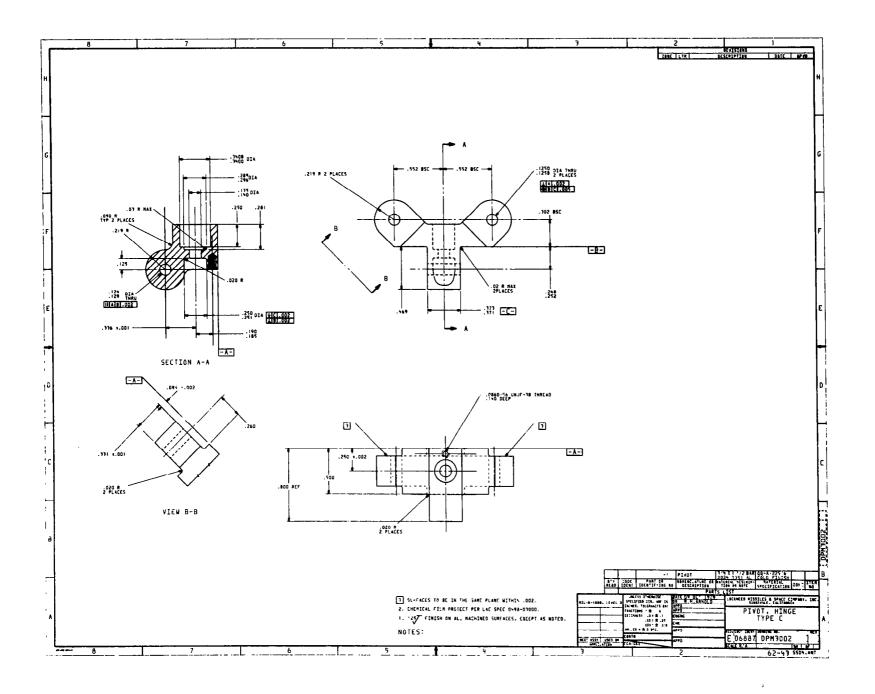


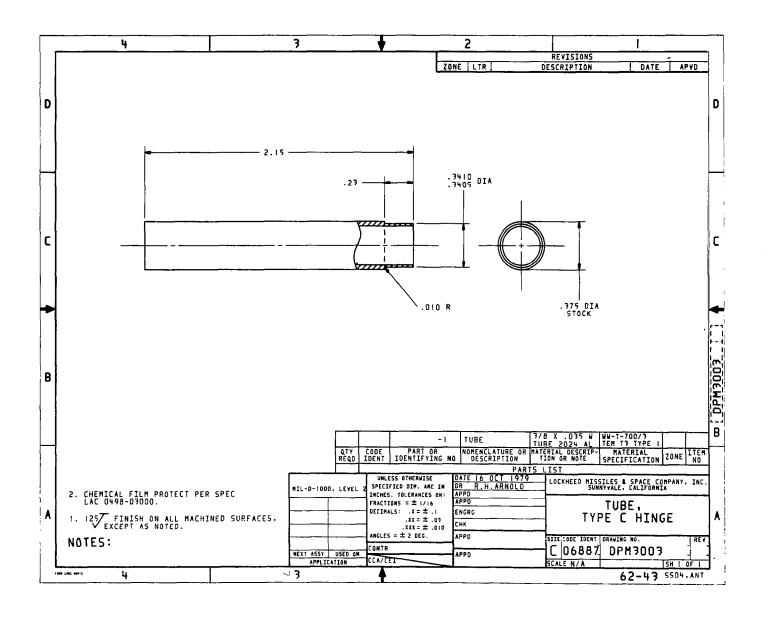


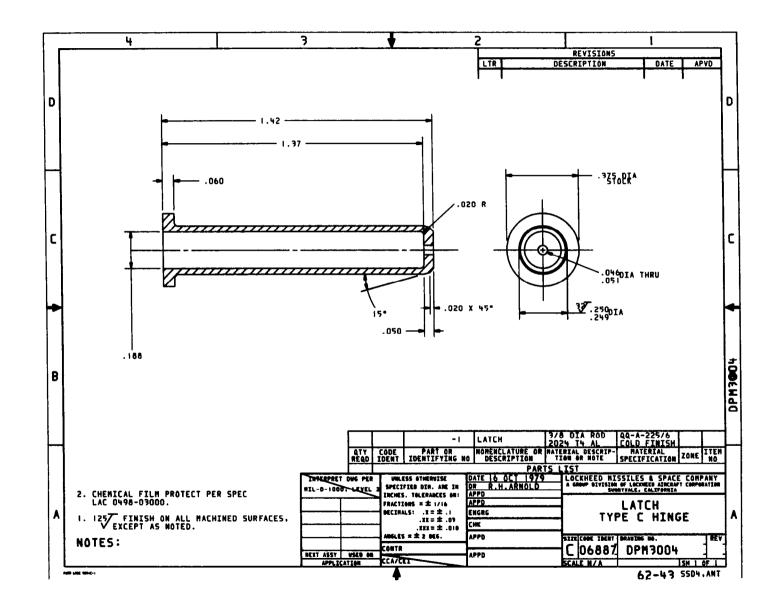


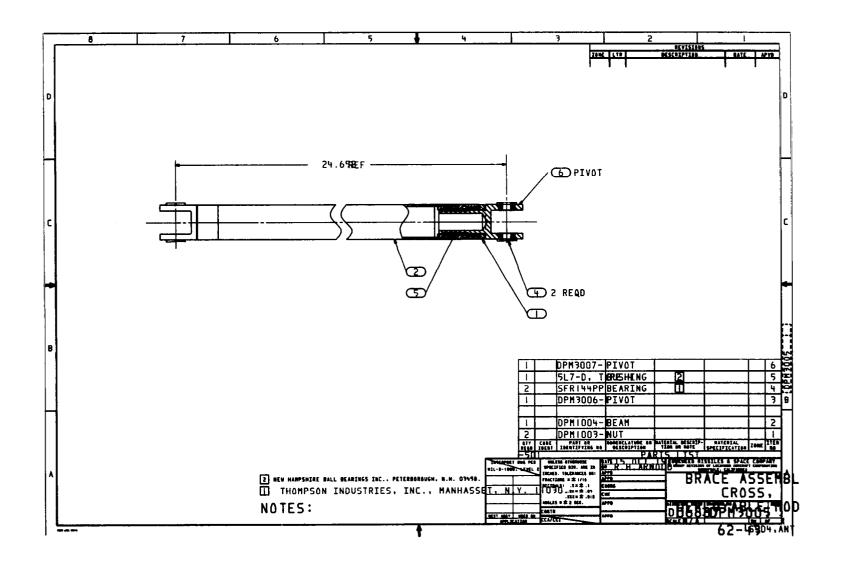


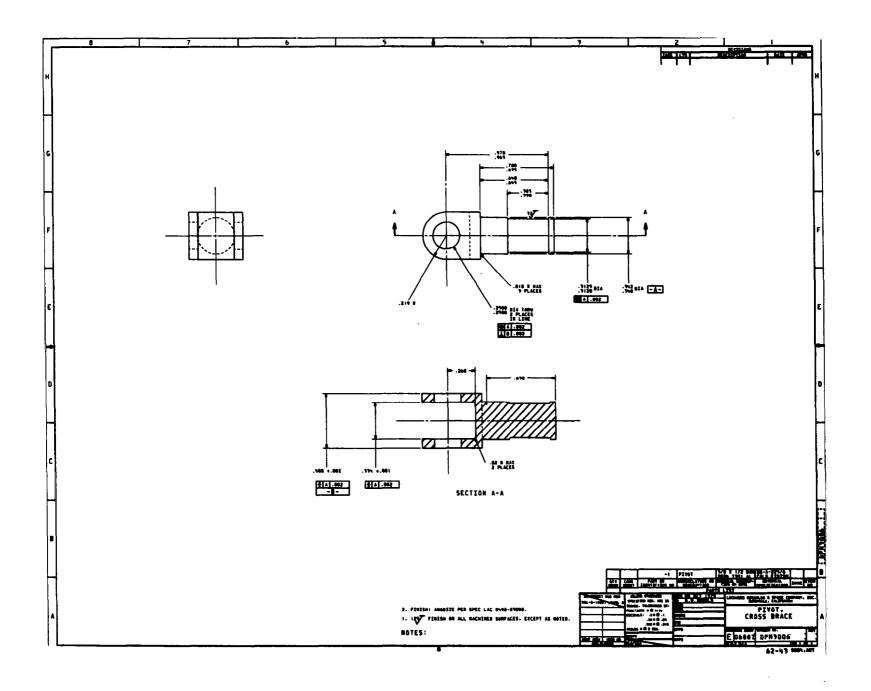


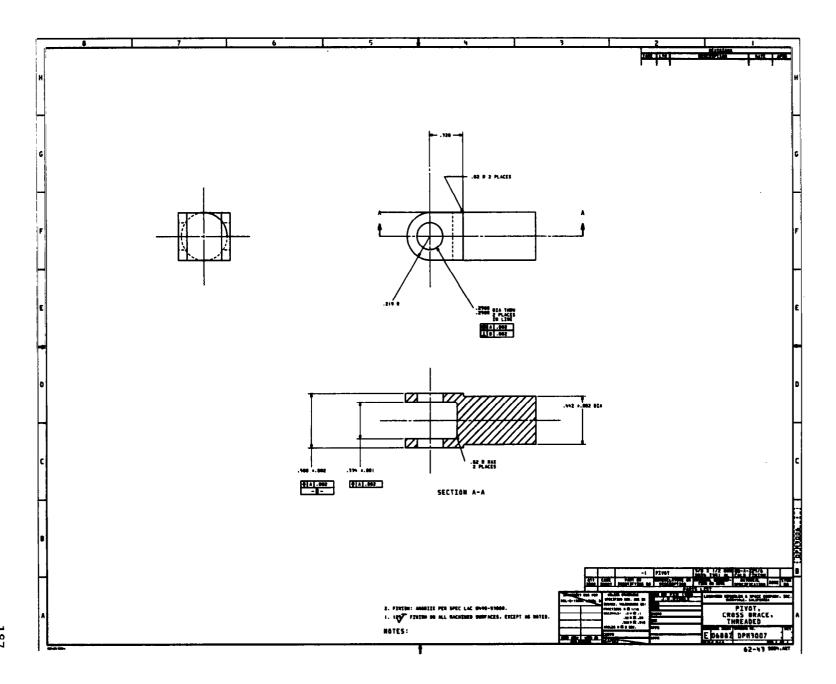


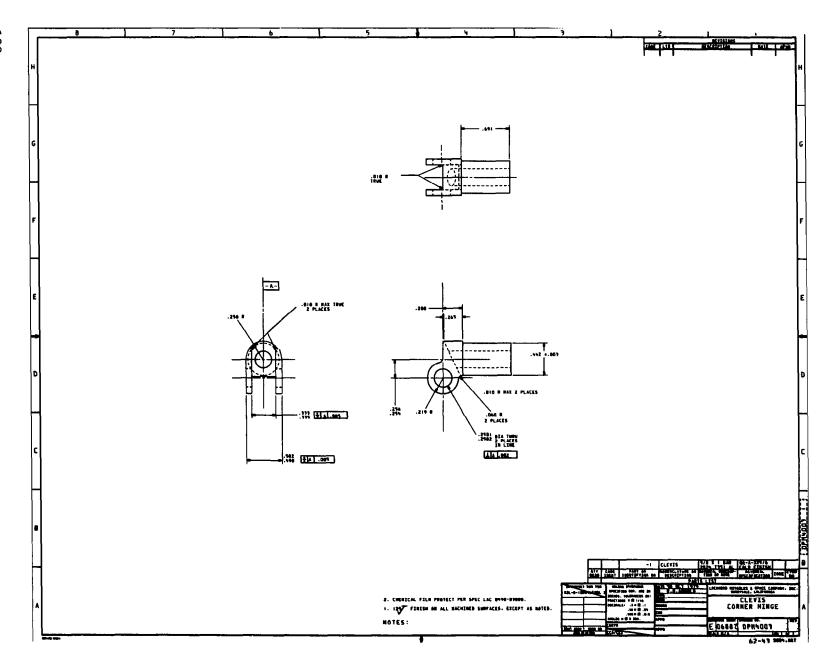




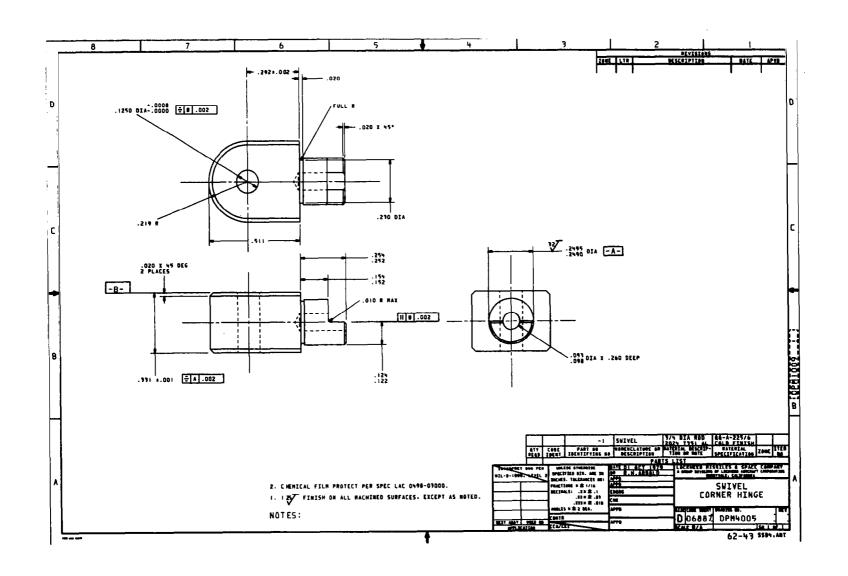


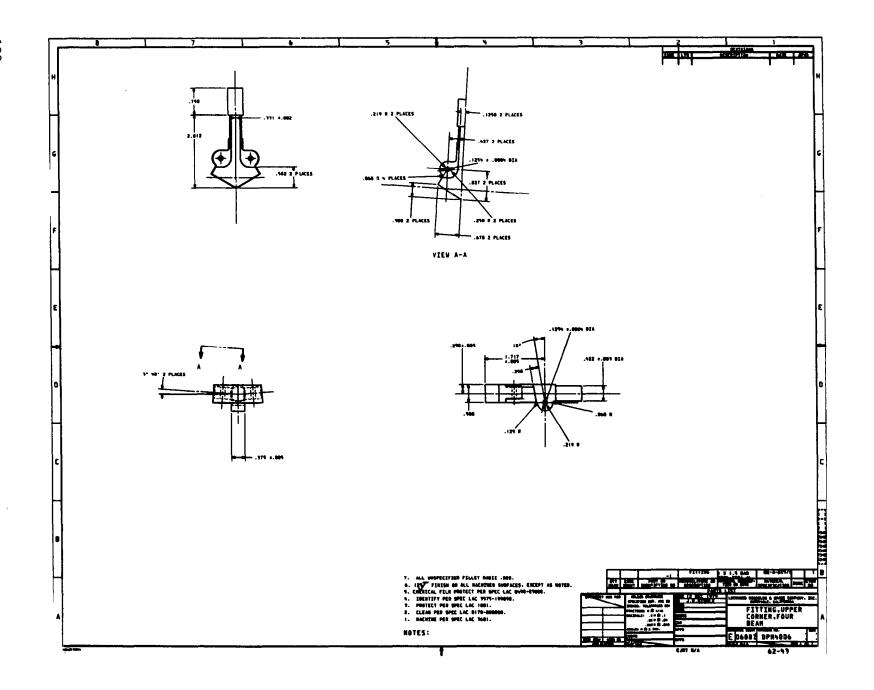


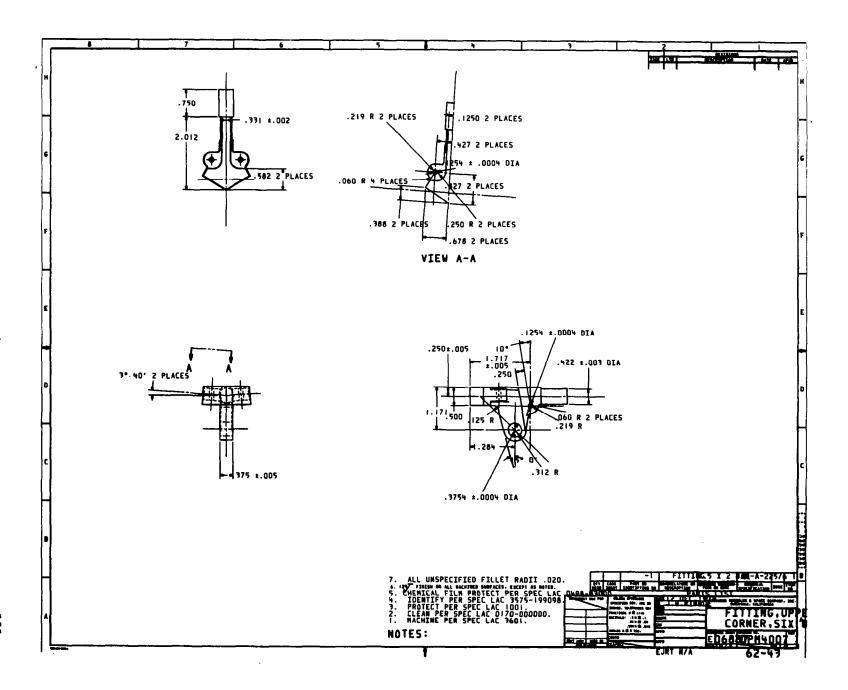




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| | | | 10. Worl | k Unit No. | |
| 9. Performing Organization Name and Add | | | | | |
| Lockheed Missiles and Space Company, Inc. 1111 Lockheed Way | | | 11. Cont | tract or Grant No. | |
| Sunnyvale, CA 94086 | | | NAS | 1-14887 (Task 14) | |
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| 12. Sponsoring Agency Name and Address | | | | · | |
| National Aeronautics and Space Administrati | | ion | ion | tractor Report | |
| Washington, DC 20546 | | | 14. Sponsoring Agency Code | | |
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| 15. Supplementary Notes | | | | | |
| Langley Technical Monitor: Harold G. Bush | | | | | |
| Final Report - Task 14 | | | | | |
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| 16. Abstract | | | | | |
| This report documents a study which researched the mechanical design of a modular | | | | | |
| antenna using a particul | | | | | |
| sufficiently to allow ma | nufacture of a wor | king demo | onstration mode | el of a module, | |
| and to predict mass properties and to make performance estimates for antenna | | | | | |
| reflectors composed of these modules. | | | | | |
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